KAPOETA EAST INNOVATIVE COMMUNITY WATER RESOURCES MANAGEMENT RAPID ASSESSMENT

SCOPING REPORT



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Scoping Report

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Table of contents

List of acronyms and abbreviations Error

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List of Figures				
List	of Tables	6		
1	Introduction	7		
1.1	Background	7		
1.2	Area description	7		
1.3	Sweco's scope of work	7		
1.4	Field assessment schedule	8		
1.5	Climate and hydrology	8		
1.6	Geology, Hydrogeology and Water Quality	10		
1.7	General introduction to the small-scale water supply options assessed	15		
2	Field assessments - Lotimor	25		
2.1	Lotuko	25		
2.2	Nakore	32		
2.3	Nanyangapokoy	35		
2.4	Lotimor village	40		
2.5	Riverbed Lotimor	41		
3	Field assessment - Upper Plateau	45		
3.1	Lokengot	45		
3.2	Nakedengoro	46		
3.3	Kaloreng	50		
4	Field assessment – Nanyangachor	59		
5	Recommendations	60		
5.1	General recommendations	60		
5.2	Recommended pilot interventions	61		
6	References	62		



List of Figures

FIGURE 1 WATER TYPOLOGIES FOR DEVELOPMENT (FROM SCHONBERGER, S. & WIJNEN, M., 2018)	7
FIGURE 2. RIVER CATCHMENT AREAS IN THE STUDY AREA	9
FIGURE 3. RAINFALL (MM) GREATER KAPOETA (REACH, 2021)	10
FIGURE 4. SECTION ALONG MAIN RIVER IN LOTIMOR SHOWING HETEROGENITY IN LAYERS, FROM FIN GRAINED SOILS TO BOULDERS	
FIGURE 5 GEOLOGY OF THE PROJECT AREA (SOURCE BGS, 2021)	11
FIGURE 6 HYDROGEOLOGICAL MAP OF THE PROJECT AREA (SOURCE BGS, 2021).	12
FIGURE 7. VISITED BOREHOLES AND BOREHOLES WITH INFORMATION FROM BOREHOLE CERTIFICA ONLY. 14	ATES
FIGURE 8 SCHEMATIC FIGURE OF A BIRKAD (ODUOR & GADAIN, 2007)	17
FIGURE 9 SCHEMATIC CROSS-SECTION OF TYPICAL SAND DAM (RAIN, 2007)	20
FIGURE 10. SCHEMATIC CROSS-SECTION OF TYPICAL SUB-SURFACE DAM (VSF, 2006)	21
FIGURE 11 EFFECTS OF EARTH BUNDS ON VEGETATION 2018-2022 TANZANIA, (SOURCE: PLANET SNA ISSUE 51, NOV 10, 2022)	,
FIGURE 12. LAYOUT OF SEMI-CIRCULAR BUND SYSTEM	23
FIGURE 13. OVERVIEW OF THE STUDIED AREA AND THE DETAILED SITE SURVEYS THAT WERE CONDUC	CTED 24
FIGURE 14. WATER HOLE/DUG WELL APPROXIMATELY 5 M DEEP	26
FIGURE 15. THE RIVER PASSAGE THROUGH THE DYKE. ROCK CAN BE SEEN ON BOTH THE SOUTHERN S IN THE PICTURE) AND NORTHERN SIDE (RIGHT). THE DISTANCE BETWEEN THE OUTCROPPING RC APPROXIMATELY 30 M ON THE NARROWEST POINT	DCK IS
FIGURE 16. TEST PIT SITES LUTOKO.	28
FIGURE 17. TEST PIT 2	28
FIGURE 18. INFILTRATION RATES LOTUKO TEST SITES	29
FIGURE 19. PROFILE OF THE RIVERBED UPSTREAM OF THE PROPOSED SUB-SURFACE DAM SITE	
FIGURE 20. A SKETCH OF POTENTIAL LAYOUT OF A SUBSURFACE DAM AT LUTOKO	31
FIGURE 21. A CONCEPTUAL SKETCH OVER HOW A COMBINED WATER AND ECOSYSTEM MANAGEMEN APPROACH COULD LOOK LIKE IN THE DEGRADED RANGELAND OUTSIDE LOTUKO	
FIGURE 22. NAKORE BOREHOLE 2(BH2)	33
FIGURE 23. PROFILE OF THE RIVERBED UPSTREAM OF THE PROPOSED SUB-SURFACE DAM SITE	34
FIGURE 24. A CONCEPTUAL DESIGN SKETCH OF THE INTAKE FOR THE PROPOSED BIRKADS AT NAKORE	
FIGURE 25. OVERVIEW OF THE CONCEPTUAL DESIGN OF BIRKADS IN NAKORE	35
FIGURE 26 OVERVIEW VISITED SITES AROUND NANYANGAPOKOI AND LOTIMOR VILLAGES	36
FIGURE 27. THE STONES MARK THE RECOMMENDED TWO NEARBY SITES FOR A NEW BOREHOLE FOLL GEOPHYSICAL SURVEYS. COORDINATES UTM 36N N 611908, E 735417 AND N 611902 E 735406 RESPECTIVELY	
FIGURE 28. PROFILE OF GULLY BED UPSTREAM OF PROPOSED CHECK DAM WALL	
FIGURE 29. OVERVIEW OF THE PROPOSED CHECK DAM IN THE GULLY NEAR NANYANGAPOKOY	
FIGURE 30. CROSS-SECTION A APPROXIMATELY 30 M DOWNSTREAM OF DAM WALL	
FIGURE 31. CROSS-SECTION B AT CHECK DAM WALL SITE	
FIGURE 32. CROSS-SECTION C APPROXIMATELY 55 M UPSTREAM OF DAM WALL	

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FIGURE 33. CROSS-SECTION D AT THE NORTHERN INLET, APPROXIMATELY 65 M UPSTREAM OF DAM WALL 4	0
FIGURE 34. THE GENERAL PRINCIPLE OF RAINWATER HARVESTING FROM ROOFTOPS AND THE USE OF SEPARATOR AND FILTERING MECHANISMS TO TREAT THE WATER. (ODUOR A.R. GADAIN, H. M. 2007) 4	1
FIGURE 35. SURVEYED AREAS WEST OF LOTIMOR VILLAGE4	2
FIGURE 36. SCOOP HOLE 5 M DEEP, 4,70 M DEPTH TO STATIC WATER LEVEL SOUTHWEST OF LOTIMOR VILLAGE	12
FIGURE 37 SLOPE OF RIVERBED DOWNSTREAM WATERHOLE WEST OF LOTIMOR4	13
FIGURE 38 BASALT DYKE OUTCROPPING AND CUTTING OFF GROUNDWATER FLOW IN RIVERBED. ARROWS INDICATE BASALT ROCK OUTCROPS	13
FIGURE 39. SLOPE OF RIVERBED UPSTREAM OF BASALT DYKE SOUTH OF NAKORE VILLAGE4	4
FIGURE 40. DETAIL SITE SURVEYS NORTH OF LOTIMOR VILLAGE4	4
FIGURE 41. A FULLY FUNCTIONAL HAFIR OUTSIDE THE VILLAGE OF LOKENGOT.	6
FIGURE 42. RIVERBED AT SITE B IN NAYIONANGOR AFTER THE JUNCTION OF THE STREAMS	7
FIGURE 43. ROCK OUTCROP SUITABLE FOR SAND DAM WALL, NAYIONANGOR SITE A	8
FIGURE 44. TEST PIT AT NAYIONANGOR SITE A4	8
FIGURE 45. PROFILE OF THE RIVERBED AT NAYIONANGOR SITE A MEASURED FROM THE FOOT OF THE PROPOSED SAND DAM WALL, NAYIONANGOR SITE A	19
FIGURE 46. CROSS-SECTION OF VALLEY AT DAM WALL SITE, NAYIONANGOR SITE A	9
FIGURE 47. PROFILE OF THE RIVERBED AT NAYIONANGOR SITE A WITH INDICATIONS OF LEVEL OF POTENTIAL SAND ACCUMULATION UPSTREAM (168 M ³ OF WATER CAN BE STORED IN THE SAND DAM)5	
FIGURE 48. RIVER WALL LIMESTONE KALORENG SITE B5	51
FIGURE 49. WATER HOLE DUG INTO LIMESTONE. NOTE THE VERTICAL SIDES OF SOFT TOPSOIL OF THE RIVERBED BEHIND	52
FIGURE 50. SOIL PROFILE IN SCOOP HOLE, KALORENG SITE B5	52
FIGURE 51. PROFILE OF THE RIVERBED AT KALORENG SITE B MEASURED FROM THE FOOT OF THE PROPOSED SAND DAM WALL5	53
FIGURE 52. CROSS-SECTION DAM WALL, WEST-EAST5	3
FIGURE 53. CROSS-SECTION 20 M UPSTREAM FROM DAM WALL, WEST-EAST5	4
FIGURE 54. CROSS-SECTION 40 M UPSTREAM FROM DAM WALL, WEST-EAST5	4
FIGURE 55. CROSS-SECTION 100 M UPSTREAM FROM DAM WALL, WEST-EAST	5
FIGURE 56. CONCEPTUAL SKETCH OF THE INITIAL STAGE OF A SAND DAM AT THE KALORENG SITE (THE DAM HEIGHT IN THE PICTURE IS AROUND 1,5 M). PLANNED FINAL TOTALL DAM HEIGHT IS 3,5 M	6
FIGURE 57. PROFILE OF THE RIVERBED AT KALORENG SITE B WITH INDICATIONS OF LEVEL OF POTENTIAL SAND ACCUMULATION	
FIGURE 58. THE WIDTH AND POSITION OF THE FIRST FLOOD SPILLWAY (MADDRELL, S., NEAL, I., 2012)	8
FIGURE 59. RELATION BETWEEN DAM WIDTH AND HEIGHT (MADDRELL, S., NEAL, I., 2012)	8
FIGURE 60. OVERVIEW OF SITE SURVEY IN NANYANGACHOR5	9

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List of Tables

TABLE 1 BOREHOLES IN UPPER PLATEAU AND LOTIMOR AREAS	12
TABLE 2. ELECTRICAL CONDUCTIVITY IN VISITED BOREHOLES DURING FIELD VISIT IN JAN-FEB 2023. WHO STANDARD FOR DRINKING WATER IS 400 MS/M (WHO, 2022) AND SOUTH SUDAN STANDARD 150 MS (UNICEF, 2008.)	
TABLE 3. SMALL SCALE SURFACE WATER HARVESTING TECHNIQUES	16
TABLE 4. LARGER SCALE SURFACE WATER HARVESTING TECHNIQUES	17
TABLE 5. EXAMPLES OF GROUNDWATER HARVESTING TECHNIQUES.	18
TABLE 6. EXAMPLES OF STORAGE/DISTRIBUTION TECHNIQUES.	21
TABLE 7. DESCRIPTION OF SITES FOR INFILTRATION TESTS	29
TABLE 8 STORAGE VOLUME FOR DIFFERENT DAM WALL HEIGHTS, KALORENG SAND DAM. CALCULATED WI MEASURED DRAINABLE POROSITY OF THE SAND = 0.25	

1 Introduction

1.1 Background

Sweco has been hired by the Swedish organisation PMU Interlife to perform a scoping study on water resources management in Kapoeta East, South Sudan. Two general areas have been assessed as part of this project, Lotimor and Upper Plateau in the Nanyangachor Payam (a South Sudanese administrative level). The two areas have very poor quality of roads which causes limited access by car to many villages in the area. The villages selected for the assessment (see detailed description below) were chosen by PMU's local partner Across based on their assessed priority of water shortages in the villages.

Across has been working with the local communities in these areas since 2018, so their knowledge around priorities have been crucial when it has come to making priorities among different areas to assess. Their work has involved humanitarian support and development projects focusing on improved agricultural practices such as the introduction of Zaï pits (see description below).

Water is a key to sustainable development and health. Different options for water resources include groundwater, surface water and non-conventional sources (e.g. desalination, reuse of wastewater, rainwater harvesting). See Figure 1. This rapid assessment has included all these different options.



Figure 1 Water typologies for development (from Schonberger, S. & Wijnen, M., 2018)

1.2 Area description

Kapoeta East county lies in the latitude N 05 19' 7.28" and longitude E 034 37' 14.90" with an elevation of 567.4 meters above sea level. It is the second largest county after Magwi in Eastern Equatoria state with the population of 274,205 disaggregated by payam as 14,339 for Jie, 39,997 for Katodori, 85,815 for Kauto, 23, 074 for Lotimor, 53,193 for Magos, 45,961 for Narus, and 11,826 for Natinga. The county borders Ethiopia to the East, Kenya to the South, Jonglei state to the North, and Kapoeta North, Budi and Kapoeta South to the West. This County is inhabited by the Toposa, Jie and Nyangatom ethnic groups. The County is located in the semi-arid regions of South Sudan. Whilst grassland and shrubland are the predominant land cover, soils are suitable for crop farming, however, climatic conditions severely limit yields, forcing households to typically follow agro-pastoral livelihoods. Agro-pastoralist practices are heavily influenced by fluctuations in climate. In the western part of the region, rainfall usually peaks in July, starting to drop in October, whilst in most parts of Kapoeta East, rainfall peaks in April and remains relatively steady through to September / October.

1.3 Sweco's scope of work

The scope of Sweco's work has been the following:

- Remote sensing/GIS analysis of the project area using available data
- Field visit to assess the local conditions including topography, geology, soil conditions, hydrology, hydrogeology



- On-site capacity building of Across local staff
- Recommendations on interventions to improve water security in the area given the site-specific conditions (water harvesting, small scale managed aquifer recharge, check dams, nature-based solutions etc)
- Preliminary identification of sites suitable for implementing pilot projects
- Basic design principles of suggested interventions
- Recommendations on pilot projects

It should be noted that the assignment has been short, and it has not been part of the scope to perform detailed studies or detailed designs and costing. Sweco's main input has been in the field work (as agreed with PMU); therefore, the time has also been limited for comprehensive reporting.

Sat	21	Travel to Kapoeta			
Sun	22	Preparation meeting	Preparation meeting		
Mon	23	Travel to Nanyangachor			
Tue	24	Morning	Travel to Lotimor		
		Afternoon	site survey		
Wed	25	morning	site survey		
		afternoon	detailed assessment		
Thu	26	morning	detailed assessment		
		afternoon	Back to Nanyangachor		
Fri	27	morning	hike to dam sites		
		afternoon	Travel to Plateau		
Sat	28	morning	site survey		
		afternoon	site survey		
Sun	29	morning detailed assessme			
		afternoon	Back to Nanyangachor		
Mon	30	morning	Site survey river		
			Nanyangachor		
		afternoon	Estimation of porosity of		
		-	soil samples		
Tue	31	morning Travel to Kapoeta Sou			
Wed	1	Reporting			
Thu	2	Flight to Juba			
Fri	3	Flight to Addis			
Sat	4	Back in Stockholm			

1.4 Field assessment schedule

1.5 Climate and hydrology

The Nanyangachor, Lotimor and Greater Plateau area has a semi-arid climate with a distinctive dry period from December to February with high temperatures (up to around 38-40 degrees). The average rainfall 1981-2021 and specific rainfall for 2021 from Greater Kapoeta can be found in Figure 3. However, the average rainfall for Upper Plateau and Lotimor is likely to be less than this. A study by NIRAS (NIRAS, 2019) indicated that these semi-arid areas receive approximately 300 to 600 mm of rain This span is verified by studies by the British Geological Survey as well (Earthwise, 2022) with indications of 400 to 600 mm, and therefore the 400 to 600 mm is assumed to be a valid span for the area and detailed enough for the scope of this study. There are three main catchment areas that drains runoff into three directions (Figure 2), all three rivers are seasonal with flows occurring during the rainy season but with some of the sub reaches only experiencing flow during major rain events and for short durations (a couple of days, according to local community members).





Figure 2. River catchment areas in the study area.

Parts of Greater Kapoeta have during the last couple of years experienced exceptionally dry conditions, and rainfall has been reported to be lower than average (a meteorological drought). The rainy season in Lotimor starts around March and peaks in April and remains relatively steady through to October/November, and it can be assumed that rainfall patterns follow more or less the same trend on upper plateau. This has led to reduced harvests, less pasture for cattle, as well as reduced availability of wild foods and surface water, resulting in large scale movement of people. When the rain comes it has often resulted in extreme events with heavy flooding as a result (Reach, 2021). This trend has been witnessed and verified by PMU's partner organisation Across in the areas where they work around Lotimor and Upper Plateau.

Even though the Reach report shows that precipitation has in fact increased across Greater Kapoeta, temperatures are also rising. This development will most likely lead to higher evapotranspiration and reduced moisture retention (the Reach report shows that soil moisture has dropped significantly in the last 20 years), resulting in lower harvests and poorer food security over time. Natural vegetation growth will in the same way be affected by reduced soil moisture over time, with negatively affected ecosystems in the area as a result.



Figure 3. Rainfall (mm) Greater Kapoeta (Reach, 2021).

1.6 Geology, Hydrogeology and Water Quality

The surveyed areas (Lotimor, Upper Plateau and Nanyangachor valley) differ from each other when it comes to topography and geology.

The geology in the Lotimor and Nanyangachor valleys consists of quartenary-tertiary unconsolidated alluvial sediments. Fine-grained silt and fine sand layers are intercalated with layers of gravel and large boulders from historical river deposits forming a heterogenic stratigraphy, see Figure 4. The presence of coarse-grained soils as well as water holes used for water supply indicates that groundwater can be available in the sediments also outside of the current riverbed itself if it has hydraulic contact through permeable layers. Groundwater recharge in the riverbed is expected to be much higher than in the other parts of the valley where heavy rain often creates surface flow with relatively low infiltration.



Figure 4. Section along main river in Lotimor showing heterogeneity in layers, from fine-grained soils to boulders.

The upper plateau is located at an elevation of approximately 1100-1160 metres above sea level (masl), approximately 400-500 meters above the surrounding main valleys of Nanyangachor and Lotimor.



According to the limited geological data available, the geology consists of tertiary volcanics (basalt) which overlays sedimentary rocks like limestone that outcrops at some locations where the basalt has eroded. See geological map in Figure 5. At the upper plateau the soil layers are thin and bedrock outcrops are common.

Several villages are located close to the edge of the plateau and the water divide where the size of the catchment areas are small and water supply options limited with no streams and very low groundwater potential.



Figure 5 Geology of the project area (source BGS, 2021).

1.6.1 Hydrogeology

The hydrogeological information from the area is very limited. The most up to date source is the hydrogeological map from BGS (2021). In the project area this seems to be based largely on the hydrogeological map of Sudan from 1989. It indicates 'low to high' groundwater potential in the unconsolidated sediments in the Lotimor and Nanyangachor valleys and 'very low to high' potential in

the volcanic areas (basalt covered areas like the Upper plateau). The latter has high potential if a borehole successfully targets a water bearing fracture or structure with a large catchment area



Figure 6 Hydrogeological map of the project area (source BGS, 2021).

Across has access to five borehole certificates (see Appendix 1). From data gathered during Sweco's field visit and information from Across staff following details on the boreholes at upper Plateau and Lotimor have been compiled. See Table 1 and Figure 7.

Borehole	Area	Total depth (m)	Depth of pump (m) / Number of rising mains	Status Jan 2023	Electrical Conductivity (mS/m)	Borehole Certificate
Kaloreng	Upper Plateau	100	57/19	Functional	121	
Namololonyit	Upper Plateau	85	54/18	Functional		Yes
Lorimo	Upper Plateau	100	60/20	Functional		Yes
Nayionanangor	Upper Plateau	100	60/20	Non- functional, broken pump		
Pekim	Upper Plateau	100	39/13	Non- functional		
Nabelenyikube	Upper Plateau	100	84/28	Non- functional		Yes

Table 1 Boreholes in Upper Plateau and Lotimor areas



Parabuku	Upper Plateau	100	72/24	Functional		
Nakore BH1	Lotimor	100	72/24	Non- functional, dry or broken pump		
Nakore BH2	Lotimor	100	78/26	Non- functional, PVS casing dis-lodged at 63 m		Yes
Lotimor BH1 (school)	Lotimor	N/A	N/A	Functional	2600	
Lotimor BH2	Lotimor	N/A	N/A	Non- functional, platform damaged by erosion		
Lotimor BH2	Lotimor	N/A	N/A	Non- functional, no pump		
Lotimor BH4 (old catholic mission)	Lotimor	N/A	N/A	Functional	104	
Lotuko BH1	Lotimor	N/A	36/12	Functional	79	
Lotuko BH2	Lotimor	N/A	N/A	Functional	67	
Namunyogur	Lotimor	50	36	Functional		Yes
Kanele BH	Kanele (on the road btw Nanyangachor and Lotimor)	N/A	N/A	Functional		
Nanyangachor BH1 (close to Across compound)	Nanyangachor	N/A	N/A	Functional	92	
Kapoeta South water supply	Kapoeta South town	N/A	N/A		100	

The location of the visited boreholes and the boreholes where there is only information from the certificates can be seen in Figure 7.

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The borehole certificates include data on borehole construction, lithology, yield and on which depth the pump is installed. This data together with data on water quality can provide important information in the process of conceptually understanding the groundwater characteristics in an area. The limited number of certificates however makes such an analysis difficult.

An observation from Table 1 and the borehole certificates is that pump installation depth often is on average 30 m above the bottom of the boreholes, and as can be seen from the certificates, 3 of 5 boreholes had the pump installed above the main water strike. The volume below the pump inlet cannot be accessed, and it is possible that the groundwater level and the main water strike is roughly at the same level. All the boreholes have casing in PVC all the way to the bottom and it is therefore not a risk to install the pump below the main water strike or close to the bottom of the borehole. This could provide more water in some of the boreholes that are seemingly dry.

There have been attempts to drill boreholes close to the edge of the western part of the plateau where the catchment area is very small, and these boreholes have been dry. As a consequence, the women (who are responsible for fetching water) need to descend 400 m in elevation to Nyangachor village to get water. This is very time demanding and tough. Access to the plateau is extremely difficult for heavy trucks, and many drilling companies refuse to drill in the area. To be successful, boreholes must be drilled in areas with potential for a large catchment as well as geological structures.

1.6.2 Water Quality

Electrical Conductivity (EC) measures the ability of the water to conduct electricity and provides an indication on the total amount of total dissolved solids (salts and ions) in the water. Total Dissolved Solids (TDS) refers to the number of substances that have been dissolved in the liquid. These substances can include salts, minerals, metals, calcium and other compounds which can be both organic and inorganic. Fresh water has TDS values between 0-1000 mg/l. Brackish water typically contains TDS in concentrations ranging from 3000 (mg/l) to 10,000 mg/l. Saline water has TDS > 10,000 mg/l TDS. The palatability of water with a total dissolved solids (TDS) level of less than about 600 mg/l is generally considered to be good; drinking-water becomes significantly and increasingly unpalatable at TDS levels greater than about 1000 mg/l (WHO, 2022). The WHO standard for drinking water is 400 mS/m (WHO, 2022) and South Sudan standard 150 mS/m (UNICEF, 2008).

The EC in the functional boreholes was measured during the field work in the functioning boreholes and the scoop hole in Lotimor river, see Table 2. The lowest values are approx. 70 mS/m in Lotuko borehole and the scoop hole in Lotimor river which indicates a fairly low salt content. The borehole in the school in Lotimor stands out with a very high salt content and an EC-value of 2600 mS/m (TDS 13 000 mg/l) which indicates saline water. There are no negative health effects from drinking the water, although the taste is rather unpleasant for humans. There is no information on the depth of Lotimor BH1 but a qualified guess is that it penetrates a deeper part of the aquifer and reaches groundwater that is affected by rock-water interaction with rocks with high salt content. Brackish groundwater is not uncommon in the Umm-Ruwaiba unconsolidated aquifer in Eastern South Sudan (Goes, 2022).

Table 2. Electrical Conductivity in visited boreholes during field visit in Jan-Feb 2023. WHO standard for drinking water is 400 mS/m (WHO, 2022) and South Sudan standard 150 mS/m (UNICEF, 2008.)

Borehole	Area	Total depth (m)	Electrical Conductivity (mS/m)	Total Dissolved Solids. TDS (mg/l)
Kaloreng	Upper Plateau	100	121	605
Lotimor BH1 (school)	Lotimor	N/A	2600	13000
Lotimor BH4 (old catholic mission)	Lotimor	N/A	104	520
Lotuko BH1	Lotimor	N/A	79	395
Lotuko BH2	Lotimor	N/A	67	335
Nanyangachor BH1 (close to Across compound)	Nanyangachor	N/A	92	460
Kapoeta South water supply	Kapoeta South town	N/A	100	500
Scoop hole, Lotimor river	Lotimor		68	340

1.7 General introduction to the small-scale water supply options assessed

The following summary is for orientation purposes only, and for details regarding advantages and disadvantages of different solutions, please see e.g. RAIN (2007), Maddrell & Neal (2012), Mekdaschi & Liniger (2013), WOCAT (2007), WOCAT (2011) and Oduor & Gadain (2007).

1.7.1 Surface water

Surface water can be collected through several different techniques and a selected number considered for this assignment are listed in Table 3 and Table 4. A general disadvantage with any kind of surface water storage is the great evaporation loss, but surface water storage is particularly important to consider for small scale infrastructure in semi-arid climates such as the one in Lotimor and Upper Plateau.



Rainwater harvesting is a useful technique to take advantage of already present structures such as tin roofs, thatched roofs, gutters etc. The technique usually leads water from a roof via gutters into a storage tank next to the building but could also be used on other structures (paved surfaces or other hardened surfaces). The efficiency of tin roofs is generally considerably higher than thatched roofs. For further details on rainwater harvesting and buildings see e.g., Mekdaschi & Liniger (2013)

Туре	Short description	Advantage/Weakness
Small surface water	Small dam(s) (single or in	Pro:
dams	cascades) to store surface water, potentially gravity fed piping	Easy access
	system to the valley	Con: high evaporation loss
		Risk of water contamination
		Pump needed to supply plateau
Check dams	Reduce erosion	Pro: good for erosion control
 Gabions Local material wood, clay 	Increase infiltration	Cons: Small or no storage of water
Birkad	Small reservoir dug in the ground,	Pro:
	usually lined with clay or cement to prevent infiltration losses	Can be protected from livestock
	Can be recharged through collecting surface flow in a local	When lined in a proper way losses to infiltration are negligible
	catchment	Cons:
	Divert from river	Evaporation (if not covered)
		Malaria mosquito breeding?
Rainwater harvesting	Very suitable and simple	Pro: easy to implement
from rooftops	technique to collect rainwater from tin rooftops	Cons: not as efficient with thatched roofs

Table 3. Small scale surface water harvesting techniques.

Box 1

Birkad

Birkads are common in parts of Somalia and Ethiopia. They are reservoirs lined with cement or clay dug into the ground. Most are large rectangular, elongated basins with vertical walls and a capacity of several hundred cubic metres, sometimes three to four metres deep. The walls and bottom are often covered in brick and/or coated with cement to reduce water loss due to infiltration to groundwater. At the top, they are open but often covered with canvas to reduce evaporation, or (in poorer villages) with nets on which is laid anything that provides shade (branches, straw, etc.).

Birkads fill naturally in the rainy season. They are placed in locations where small streams form during rain, which are then routed to the birkad with dug trenches. A birkad can sometimes be filled in a few hours. In villages with poor water availability, feed channels can be a few kilometres long, and take the form of proper canals coated with cement and/or covered. Birkads are often clustered





Туре	Short description	Advantage/Weakness
Hafir	Large volume – water supply, livestock, irrigation, can be recharged via channel surface flow, silt and sand traps will reduce the sedimentation in the Hafirs and prolong the lifetime of the structure.	Labour intensive Water losses - Evapotranspiration Contamination – difficult to keep livestock from entering the hafir Damage due to flash floods etc Siltation
Dams	Large volume – water supply, livestock, irrigation, correct siting and design is very important	Dam failure – big consequences Siltation Costs

1.7.2 Groundwater

Groundwater is used for water supply throughout the Horn of Africa (HoA) region and forms the sole source of water for most communities in the borderland areas. The widespread food and livelihood insecurity and poverty means an expanding role for groundwater in resilience building in borderland communities given the pressing challenges of climate change. Due to climate change traditional sources of surface water become scarce, and groundwater has the greatest potential for positive development impact in the forty percent of Sub-Saharan Africa classified as 'drylands' (Schonberger, S. & Wijnen, M., 2018)

Groundwater is present in shallow aquifers, e.g., alluvial aquifers along riverbeds, and in deep rock aquifers. The amount of groundwater available depends on several different factors i.e., type of sediments or rock, geological structures, topography, recharge etc. Alluvial aquifers in riverbeds with coarse sediments can be recharged in connection with sparse runoff events in the river, while recharge to deeper rock aquifers in arid climates can be in the magnitude of 5-10 mm/year implying that large recharge areas are needed to allow sustainable yields avoiding groundwater mining and depletion of the groundwater table.

Groundwater is often the last resource available during prolonged drought periods. A conjunctive use of different water sources will lessen the pressure on the deep groundwater resources that have very low rates of recharge and are susceptible to overuse. Examples of conjunctive use of water sources could be initial use of rainwater harvested directly after the rainy season (e.g., hafirs and birkads) followed by sand dams and finally when these sources have dried out, dug wells and last deep boreholes (Sweco, 2021).

Туре	Short description (reference)	Advantage/Weakness	
Spring protection	Interventions to cover and protect springs and allow for safe access	<i>Pro:</i> Increased accessibility Protect from pollution	
		<i>Cons:</i> Springs can be seasonal	
Improved shallow wells – hand dug	Dug wells lined with well rings or masonry to prevent from collapsing and allowing wells to be dug deeper. Also provides protection through cover and can be installed with hand pump	Pro: Does not need heavy machinery like drilling rigs Use of casted concrete well rings allow hand dug wells to be dug deep without risks of collapsing walls Provides protection Can be issued with hand pump – but if pump is broken water can still be accessed with a bucket Cons: Time consuming and strenuous work to construct Only viable in non-consolidated sediments	
Manual drilling	Manual drilling of wells is a low-cost technology that has been introduced successfully in several African countries but is not widespread in the HoA region. Manual drilled wells can reach down to 30 - 40 m depth in unconsolidated aquifers	<i>Pro:</i> Low cost Can be done with simple equipment <i>Cons:</i> Works only in unconsolidated aquifers Limited depth	

Table 5. Examples of groundwater harvesting techniques.



Managed Aquifer Recharge	Intentional recharge of water to aquifers for subsequent use or environmental benefit. MAR offers numerous benefits, including storage to improve security of water supply, including long-term storage for drought supply. Siting and suitable sediments in an important factor.	 <i>Pro:</i> Protects stored water from evaporation Can be done with simple methods if conditions are suitable <i>Cons:</i> Can be challenging to find suitable sites Regular maintenance of recharge infrastructure needed
Subsurface dams	System to store groundwater by a "cut-off wall" (dam body) set up across an aquifer in a riverbed. Siting very important Shallow sediments in riverbeds Build on existing natural barrier to GW flow if possible Clay or masonry Access can be improved through e.g. Infiltration gallery + collector well protected from flood.	<i>Pros:</i> Cheaper and less vulnerable than sand dams <i>Cons:</i> Risk of contamination from livestock
Sand dams	A reinforced stone masonry or concrete wall built across a seasonal sandy river. During flow events the dam is gradually filled with sediments and water creating an artificial aquifer. Siting very important Access can be improved through e.g. Infiltration gallery + collector well protected from flood	 Pros: Can be only feasible solution in some areas Less losses to evaporation compared to normal dams Cons: Failure rate high in e.g. Kenya Risk of failure during flash floods Siltation – the conditions regarding sediment transport must be right Sustainability – quality of works Risk of contamination from livestock
Borehole	Borehole drilled into sediments or rock.	Pros: Can be only viable solution Often the last resource to dry out during drought <i>Cons:</i> Needs special machinery Expensive If pump breaks water cannot be accessed



Siting very important - dry borehol common

Box 2

Sand dams

Sand dams are a simple, low cost and low maintenance, replicable rainwater harvesting technology. They provide a clean, local water supply for domestic and farming use and are suited to arid and semi-arid areas. Sand dams have been used extensively in parts of Kenya. Failure rates can be high if the local conditions are not suitable, notably the dam can be filled with silt and mud instead of sand.

A sand dam is a stone masonry barrier across a seasonal sandy riverbed that traps rainwater and sand flowing down the catchment. A sand dam is typically 1 - 5 metres high and 10-50 metres across. When it rains the dam captures the sediment carried by the water – the sand in the water sinks to the bottom, whilst the silt remains suspended in the water and overflows. Eventually the dams fill with sand -sometimes after only one rainfall or over 1 - 3 seasons. The sand dam creates an artificial groundwater aquifer, depending on the particle size of the sand 10-30% of the volume of the sand dam can hold water.

Sand dams require careful maintenance and immediate repair if necessary. If there are risks of flooding, water can spill over the wing walls and erode the riverbanks during heavy rains and flash floods. However, this risk can be eliminated through careful siting and design of the sand dam (when riverbanks are made of solid rock),



Figure 9 Schematic cross-section of typical sand dam (RAIN, 2007)

Sub-surface dams

A subsurface dam intercepts or obstructs the flow of an aquifer and raises the groundwater table upstream of the structure. It also reduces the variation of the level of the groundwater table. A subsurface dam is constructed below ground level and arrests the flow in a natural aquifer (most often the groundwater flow in a sandy riverbed). The best sites for construction of groundwater dams are those where the soil consists of sands and gravel, with rock or an impermeable layer at a few metres' depth. Ideally, the dam should be built where rainwater from a large catchment area flows through a narrow passage. A sand dam creates an artificial aquifer whilst a sub-surface dam enhances and strengthens an already existing aquifer.



1.7.3 Storage – distribution

Sometimes water can be accessed and used directly (e.g., from a borehole, dug well, spring or sand dam). There are situations when water needs be stored for longer time, e.g., when collecting water from a tin roof.

In the project area livestock is the lifeline of the population. To avoid contamination of the water source it is important to plan for separate distribution for livestock and humans.

Туре	Short description	Advantage/Weakness	
Hand pumps	Very common in rural areas in Africa and Asia. Normal models can pump water from 0-45 m depth, but special models can pump from 90 m depth.	Pros:	
		No electricity needed	
		Usually available locally	
		Cons:	
		O&M demands skills	
		Access to spare parts	
Solar pumps	Electrical submersible pumps ran on solar power	Pros:	
with elevated tank		Cheaper than diesel pumps	
		Less susceptible to breakdown than diesel pumps	
		Less O&M than diesel pumps	
		Cons:	
		Initial costs	
		O&M can be a challenge	
		Theft + vandalism	
		Can be risk of aquifer depletion	

Table 6. Examples of storage/distribution techniques.

Ferrocement tanks	Ferrocement consists of a cement- rich mortar reinforced with layers of wire mesh, sometimes with additional plain wire reinforcement for added strength. Tanks made of ferrocement are used in many countries for the collection and storage of water for drinking, washing, for animal use and irrigation	Pros: Relatively cheap Flexibility in shape <i>Cons:</i> Labour intensive
Storage tanks for rainwater harvesting	Tanks to store rainwater collected from e.g. roofs. Often made in plastic, concrete or ferrocement	

1.7.4 Nature Based Solutions for sustainable land and water management

Improved water management should go hand in hand with sustainable land management. An area affected by increased drought will experience reduced available soil water content which will affect the ecosystem in a negative direction, a negative trend that has been observed in the target area during the last 20 years (Reach, 2021). This development can be reversed by the adoption of nature-based solutions for sustainable land and water management such as terracing (known as fanya juu and fanya kii in Swahili), protection of riparian areas, area closures for rehabilitation as well as Zai pits (a technique that Across has already started to implement in the project area, see description in the box below). These solutions are simple techniques to increase the natural processes of water infiltration and natural regeneration. Another example is the use of earth bunds that are dug-out halfmoon shaped pits (see description in box below) in patterns across the landscape to reduce the speed of runoff and thus reducing erosion and increasing infiltration. Examples from trial sites have shown considerable effects on restoration of degraded rangelands. See Figure 11. The step from implementing Zaï pits to the implementation of earth bunds is very small, and therefore it is recommended that this should be an integrated part of any water management activities implemented in the area. The introduction of Nature-Based Solutions should be integrated with awareness raising and training of local communities on land and water management with regards to e.g. risks of over-grazing and the importance of vegetation on reducing erosion.



Figure 11 Effects of earth bunds on vegetation 2018-2022 Tanzania, (Source: Planet Snapshots, Issue 51, Nov 10, 2022)

Box 3

Zaï pits

Planting pits or Zaï pits (the technique has different names in different countries) are mini-basins planted with a few seeds of annual or perennial crops. They are dug by hand and the excavated soil is placed downslope of the pit and sometimes formed into a small ridge to best capture rainfall and runoff. Manure and mulch are added to the pits to improve the fertility of the soil and reduce evaporation. Planting pits are applied on flat to gently sloping land (0-5%) that receives rainfall of 350-600 mm/y.

Earth bunds

These semi-circular bunds are usually made of earth or stone and have commonly a diameter of 2-8 m. The bunds are larger versions of the Zaï pits and are commonly used in arid climates for grazing land rehabilitation or fodder production. Earth bunds are built in a rotational pattern between the lines over a plot (Figure 12) and rarely used on slopes steeper than 5%.



Figure 12. Layout of semi-circular bund system (source: Mekdaschi Studer, R. and Liniger, H. 2013)

1.8 Overview of site surveys conducted

The figure below shows the locations of the site surveys conducted. The inset table summarises the water harvesting techniques that were assessed for each location.

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T Chart	SA yangachor	5 6A 62 63 Kaloreng 4 Lokengot/Nakedengoro			0 5 10 km
Survey site	Nearby village	Assessed water harvesting techniques	GPS coordinates	Detailed description (chapter)	
	Lutela	Hafirs, earth bunds and	(741238.35565428540576249	398	
	1 Lutoko	subsurface dam	612983.32075866183731705)	2.1	The second second
3	2 Nakore	Birkads	(737013.15289022983051836	2.2	The man with the last in the second
			615025.69241907075047493)		
13	3 Nanyangapokoy	Hafir	(734790.21090899186674505 610322.01399065251462162)	2.3	
		rooftop rainwater harvesting,	(735378.04918614099733531		Logond
4	4 Lotimor	sand and subsurface dam	609920.51863125001545995)	2.4 & 2.5	Legend
5	Lokengot/Nakedengoro/	Sand dam	(704464.153049666666735709	3.2	
5 A-t	Nanyionangor	Sanu uam	613578.26396040839608759)	3.2	Cuprov cito
	Kaloreng	Sand dam	(710921.2042128728935495	3.3	Survey site
			615541.48475994495674968)		🔶 Village
	7 Nanyangachor	Subsurface dam	(694712.22162857267539948 607760.17868958332110196)	4.1	River reaches
	Lokengot/Nakedengoro/		(704526.33734920073766261		Catchment areas
1		Existing hafirs upper plateau		3.1	

Figure 13. Overview of the studied area and the detailed site surveys that were conducted.



2 Field assessments - Lotimor

For water supply, the communities around Lotimor are dependent on dug-out wells in the riverbed of and three working boreholes around the area (two in Lotimor village and two close to the village of Lotuko). There are visible signs of dug-out wells in many places along the river, but the team could only find one where there was still available water. This gives an indication of a community that is very dependent on the available boreholes (strengthened by interviews with the different local communities and with the local partner organisation). If these would be depleted the communities would need to migrate to find water (usually across the border into Ethiopia). The conclusion after the general assessment is that the introduction of multiple sources of water (even though small in size) would help to reduce the pressure on the boreholes. The following sections describe the more detailed findings from the area around Lotimor.

2.1 Lotuko

There are two boreholes on both sides of the river. Both boreholes had been malfunctioning, but they were rehabilitated by Across and are now functional. The riverbed shows signs of being suitable for subsurface dams, a mix of boulders, gravel, sand and even silt. There is a good rock outcrop that could be used as foundation for the construction. The local community has dug several holes along the river to find water during the dry seasons. Some of these are up to five meters deep, so there are clear signs that this is place that naturally stores water. It is also suitable that it is a place where the community normally goes to find water. The sub-surface dam will help to strengthen the available groundwater stored along the riverbed. A first action to do (before construction of any dam) could be to penetrate the top layer of the riverbed (a harder more clayey layer) before the rainy season starts to allow for water to infiltrate easier into the more suitable layers underneath.

Available source(s) of water and associated technique(s)

Borehole (two boreholes by the river close to the village)

Dug out wells

General water supply situation at the time of the assessment:

Good: close access to two boreholes but vulnerable to break downs of the pumps

Potential improvements?

Construct sand dam in the riverbed (see general description of technique above)

Construct hafirs (based on the examples of Lokengot and Nakedengoro)

Construct birkads in connection to the hafirs (see general description of the technique above)

The two boreholes in Lotuko are drilled into a gneissic dyke crossing the river below the village. The river has eroded the dyke and created an opening where the river can pass. Upstream of the dyke there are several open wells / deep water holes dug into the river sediments, some up to 5 m deep. None of these contained water at the time of the site visit. The villagers had dug approximately 10 deep holes within a radius of 30 m showing that they believe that the occurrence of groundwater is very site specific. River sediments can be very heterogenous, but in general it is better to dig deeper than starting on a new hole 5 m away. The water holes contain large boulders which creates risks for the persons digging and accessing water, and there are risks of collapsing holes, see Figure 14.





The use of casted concrete well rings is not known in the area. This would allow digging of deeper wells and protection from falling boulders. It would also hinder the water holes from collapsing during floods. In e.g. Afghanistan wells are dug up to 60 m deep by hand. Large diameter dug wells are known from e.g. Niger and Pakistan and can be >100 m deep providing year-round access to water during many decades.

A sub-surface dam where the river crosses the gneissic dyke would increase the groundwater availability upstream and would allow a longer season when dug wells can be used. If casted well rings are introduced and wells can be dug deeper they might be able to provide year-round access to water. A subsurface dam would increase the groundwater table and thus could also potentially increase the recharge to the rock gneissic aquifer where the boreholes are located increasing their yield.

Figure 14. Water hole/dug well approximately 5 m deep.

2.1.1 Site investigations Lotuko sub-surface dam.

A subsurface dam should be constructed on top of the underlying bedrock or an impermeable layer and can extend up to the riverbed surface or below. The sub-surface dam can be made of clay or masonry. The sub-surface dam should be constructed on the narrowest passage between the rocks on each side of the river.

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Figure 15. The river passage through the dyke. Rock can be seen on both the southern side (left in the picture) and northern side (right). The distance between the outcropping rock is approximately 30 m on the narrowest point

2.1.1.1 Test pits Lotuko

The depth to the bedrock can be investigated using geophysical techniques such as georadar or geotechnical drilling. Neither of these methods were accessible to the project team. Three test pits were dug to assess the underlying soil and, if possible, the depth to the bedrock.



Figure 17. Test pit sites Lutoko.



Figure 16. Test pit 2.

Test pit 1 was dug 2 m from the rock outcrop on the southern part of the river (see Figure 17). The first 0,25 m consist of a relatively hard pan of silt, sand and gravel. From 0,2 m to 0,85 m the material consists of unsorted sand, gravel and boulders. The bedrock was not reached in spite of the close distance to the outcrop which indicates that it has a steep inclination.

Test pit 2 was dug 7 m from the rock outcrop on the southern part of the river. Under a 0,25 m relatively hard pan of silt, sand and gravel the material consisted of well sorted coarse sand, gravel and boulders up to 0,2 m in diameter down to 1.2 m depth (Figure 16). It is obvious that the material has been transported for some time before being deposited during rather high water velocity. The bedrock was not reached during digging and a 2 m iron rod was hit into the bottom of the pit to verify potential presence of bedrock. The iron rod did not reach the bedrock and it can be concluded that the riverbed must be >2.4 m deep.

Test pit 3 was dug 12 m from the rock outcrop on the southern part of the river. Under the 0.2 m pan sand, gravel and boulders were encountered. The total depth of test pit 3 was around 0.8 m.

2.1.1.2 Infiltration tests, Lotuko

Three infiltration tests were carried out using 1 m PVC pipe with diameter 100 mm, adding water and measuring the infiltration rate. This is a simple testing method and also the number of samples is very small for a solid assessment. However, given the project approach with focus on rapid assessment of



multiple sites the results should be seen as indicative but provide a good comparison between the tested sites.

Infiltration test	Location
1	2 m upstream from test pit 2. 0,2 m below ground surface in the lower part of the hard pan (silt, sand and gravel)
2	In test pit 2 0,83 m below ground surface (well sorted coarse sand, gravel and boulders)
3	160 m upstream from infiltration test 1, 0,25 m below ground surface. The pan is less hard at this site,

Table 7. Description of sites for infiltration tests



Figure 18. Infiltration rates Lotuko test sites

The results of the infiltration tests are presented in Figure 18. Infiltration capacity in the coarse sand and gravel below the harder pan (infiltration test 2) is very high which means that recharge in this layer will help replenish the aquifer effectively. Infiltration test 1 is made in the hard pan itself. It is not surprising that the infiltration capacity is substantially lower in this top layer of the riverbed compared to the coarse sand underneath, although it is still relatively high and it can be expected that the underlying aquifer in the coarse river bed is recharged during periods of flowing water in the river. Digging perpendicular trenches across the riverbed or patterns of small holes penetrating the pan layer would increase infiltration. This could be done upstream of the area where the community has dug water holes, although they would be clogged after each rainy period.

2.1.1.3 Slope of riverbed, Lotuko

The slope of the riverbed upstream of the proposed subsurface dam site was measured, see Figure 19. The riverbed has a very gentle slope on this stretch of the river and has an undulating surface where channels have eroded through piles of sand and boulders. The average slope 230 m upstream of the sub surface dam site is only approximately 0.6%.



Figure 19. Profile of the riverbed upstream of the proposed sub-surface dam site.

2.1.1.4 Conclusions sub-surface dam Lotuko

The presence of several water holes (dry at the time of visit) implicates periodical presence of groundwater. Coarse sand and gravel in the riverbed indicate that the groundwater storage capacity could be high. The recharge area is large (169 km²) and most probably there is groundwater available at greater depths. A sub-surface dam in the gap in the gneissic dyke that is currently partly blocking the groundwater flow in Lotuko would increase the groundwater potential upstream raising the groundwater table. This would allow the water holes to contain water during much longer periods, and if dug deep enough probably during the whole year. The subsurface dam would decrease the groundwater flow downstream. 6.5 km from the proposed sub-surface dams' site there is a basalt dyke outcropping which creates a natural sub surface dam. There are no villages between Lotuko and this dyke, and along the 6.5 km stretch of the river water will recharge the aquifer in the riverbed. This indicates that the impact on downstream water availability of constructing a sub-surface dam at this specific site would be limited.

This rapid assessment could not determine the depth to the bedrock in Lotuko. A sub-surface dam should be dug to the bedrock or an impermeable layer of clay or silt to be effective. Building a sub-surface dam is labour intensive as much digging is needed. The dam wall itself can be made of clay or masonry. There are no strong forces or pressures acting on a sub-surface dam wall, and the associated risks are small compared to a normal dam where collapse can lead to flooding and erosion. A sub-surface dam can function for decades and provide water for thousands of persons if the conditions are favourable (e.g. the water supply of Hargeysa was mainly based on a sub-surface dam between 1960-2000 approximately). It is recommended to install infiltration galleries on the upstream part of the sub-surface dam and connect these to a collector well (see Figure 20). A hand-pump can be installed to mitigate contamination, but considering the risks of pump failure, a covered access hole should also be built so water can be accessed with a bucket system as well. The collector well must be well protected from flooding.



Figure 20. A Sketch of potential layout of a subsurface dam at Lutoko.

Sweco also recommends Across and PMU to consider introducing casting of concrete well rings. The well rings protect the current water holes from collapsing, and with techniques to dig inside the well rings, they can reach much deeper allowing for more secure access to groundwater. In e.g., central Afghanistan wells are dug up to 60 m depth using this technique. An advantage with dug wells compared to boreholes is that water can be accessed without a pump. The wells can also be repaired without special machinery or tools. The sediments in the river valley in Lotimor consist of alluvial sediments where dug wells can be a feasible method to access water if sited in alluvial (river) sediments. The construction of a deeper dug well is time consuming but much cheaper than drilling of boreholes.

2.1.2 Hafirs and earth bunds around Lotuko

The rangelands around Lotuko shows signs of degradation with large erosion gullies that cross the landscape. If this development is not reversed the land will continue to lose its topsoil and the possibility for ranging cattle and farming will continue to be deprived. There are several nature-based solutions that can be used to revert the degradation, but the construction of earth bunds is specifically recommended for this case. The reason is that Zaï pits have already been introduced in the community as a technique for more drought-resistant farming and the earth bunds is a very similar technique but for larger scale, and it is specifically suitable for rangelands. The earth bunds are half-moon formed pits where the dug-out earth forms a small wall on the downstream end of the pit to slow down runoff to allow for increased infiltration into the ground. The resulting infiltration will assist to rehabilitate the vegetative ground cover, and with several earth bunds covering the landscape, the technique will help to rehabilitate larger areas of land.

Since the gullies are already formed this could be a suitable site for the construction of a hafir. The eroded gulley can be enlarged to form the hafir while upstream smaller gulley can be converted into canals increasing the water that is lead to the hafir. The hafir and the earth bunds could preferably be used in combination to include several techniques to allow for an integrated approach to landscape



restoration aligned with the ecosystem-based approach where water, ecosystem and living resources management goes hand in hand (Convention of Biological Diversity, 2021). Figure 21 shows a conceptual sketch over what this integration could look like in the attempt to reverse land degradation in the Lotuko area.

The importance of integrating all of these aspects becomes specifically apparent in an agropastoral community such as the ones around Lotimor (and Upper Plateau), where their dependence on **the water** (for domestic use and for cattle), **the land** (agriculture, food security and rangeland for cattle) and **the living resources** (agriculture, vegetation for ranging cattle and the cattle itself) in combination is very clear. Sweco recommends that introduction of Nature-Based Solutions such as earth bunds and construction of Hafirs for water harvesting should be integrated with awareness raising and training of local communities on land and water management with regards to e.g. risks of over-grazing and the importance of vegetation on reducing erosion.



Figure 21. A conceptual sketch over how a combined water and ecosystem management approach could look like in the degraded rangeland outside Lotuko.

2.2 Nakore

The village of Nakore has 2 boreholes drilled by Across. Currently both are non-functional at the time of the visit. Nakore BH1 is situated between the village and a small river. It is dry or has a non-functional pump. The borehole is 100 m deep and the pump is installed at 72 m which means that yield potentially is higher if the recharge to the borehole occurrs in the bottom 28 m of the borehole. See Table 1.

The second borehole (Nakore BH2) is located 650 m south of BH1. It is drilled to 100 m depth. The borehole PVC casing is thought to have dislocated. After the pump was ejected for reparation it could not pass 63 m depth. The yield in BH2 was lower than BH1. See Figure 22

The available water source could furthermore be strengthened by building a Birkad along the river and digging a small channel to fill this when water is flowing in the river. This could be furthered strengthened



by small check dams along the river. The water in the river only flows around 1-2 days when the rain comes, but the observations of the total flow in the river section (more than 0,5 meters on a 5-meter-wide river section) from the local community indicates that it would be enough to fill a Birkad (and maybe even several Birkads) by such an event (and there would be multiple during a normal rainy season).



Figure 22. Nakore borehole 2(BH2)

Available source(s) of water and associated technique(s)

Boreholes (firstly by the riverside in Lotuko and secondly at the school in Lotimor)

Dug out wells in the riverbed

General water supply situation at the time of the assessment:

Limited: Water is available, but the community needs to travel far (>5 km)

Potential improvements:

Refurbish boreholes (two available but not functioning)

Construct hafirs (based on the examples of Lokengot and Nakedengoro

Construct birkads in connection to the hafirs (see general description of the technique above)

2.2.1 Site investigations Nakore birkads

According to the community members, water flows in the stream several days after a rain event and results in water depths up to 40-60 cm deep. This observation indicates that the flow must be several 10's of litres per second. A topographical survey showed that it would be feasible to divert water from the stream and lead it to two flat areas of approximate size of 15x30 m and 20x40 m respectively, see Figure 25. A series of birkads could be dug and connected with channels or pipes. It is advantageous to reduce the area of the birkads to reduce losses due to evaporation. The evaporation could be further reduced by covering the birkads with sheet metal, plastic or other material. A birkad of 2.5x10x4 m (BxLxH) can store 100 m³ of water. Up to 10 birkads can be dug which would provide 1000 m³ of water, preferably for human consumption. The current water consumption per capita in Nakore is not known, but an estimation from Lotimor area based on observation is 5-10 l/person*day. A series of 10 birkads



could thus provide water for 1000 000l /10 l/p*d =100 000 person days which should cover most of the water needs for Nakore villages. Figure 24 and Figure 25 shows a conceptual design sketch of the proposed Birkads in Nakore.

If assumed that the average flow in the river during a rain event is 0.1 m³/s (100 l/s). This is a conservative estimation based on a yearly rainfall of 300 mm/year and the total yearly rainfall spread out evenly across 90 days, which is rarely the case. It is more likely that the average flow in the river will be higher during the two days of rainfall. The flow would in theory be enough to fill the ten birkads during a single rain event (a total of 0.1 m³/s * 3600 s/hour * 24 hours/day * 2 days=17280 m³). However, there are factors that will reduce the actual volume that can enter the Birkads such as what percentage of the flow that is diverted from the stream (Figure 24), losses in the canal system and the silt trap, etc. But this gives an indication that, given a number of rain events during the rainy season, the stream flow will provide enough water to fill the proposed number of Birkads.



Figure 23. Profile of the land surface between stream intake and suggested area for birkads.



Figure 24. A conceptual design sketch of the intake for the proposed Birkads at Nakore.



Figure 25. Overview of the conceptual design of Birkads in Nakore.

A rapid assessment of the conditions downstream of BH1 showed that it would be possible to construct a hafir 140 m southeast of BH1 in a natural depression. This could store water for livestock and be filled by the stream during rain events.

2.3 Nanyangapokoy

The villages of Nanyangapokoy access water through the boreholes in Lotimor approximately 1700 m away or through a water hole in the riverbed approximately 2000 m away. The village had a borehole that collapsed > 15 years ago after which the village was moved 650 m south to its current location. Catholic missionaries made geophysical surveys and recommended two suitable sites for a new borehole, see Figure 13 and Figure 26. The sites were known to the village elder who showed the sites to the project team. As reference for eventual future drilling, the coordinates are given here: UTM36N N 611908, E 735417 and N 611902 E 735406 respectively

Available source(s) of water and associated technique(s)

Boreholes (the two in Lotimor)

Dug out well in the riverbed

General water supply situation at the time of the assessment:

Ok: Water is available, but the community needs to walk to get it (1-2 km)

Potential improvements?

Construct hafirs (based on the examples of Lokengot and Nakedengoro)



Construct birkads in connection to the hafirs (see general description of the technique above)

Refurbish boreholes (two available but not functioning)



Figure 26 Overview visited sites around Nanyangapokoi and Lotimor villages


Figure 27. The stones mark the recommended two nearby sites for a new borehole following geophysical surveys. Coordinates UTM 36N N 611908, E 735417 and N 611902 E 735406 respectively

2.3.1 Site investigations Nanyangapokoy check dam site

The soft organic rich top-soil south of Nanyangapokoy villages is vulnerable to gully erosion and a system of gullies have developed. Approximately 1200 m southwest of the villages the width of the gullies are up to 14 m. At this site several small gullies converge to a larger one. This site could be suitable for a check dam built with e.g. sand bags. See Figure 13 and Figure 29.



A profile of the gully bed is shown in Figure 28.

Figure 28. Profile of gully bed upstream of proposed check dam wall

Cross-sections were measured at the proposed dam wall site, 60 m upstream, at the north inlet and 30 m downstream of the dam wall site, see Figure 29 - Figure 33.



Figure 29. Overview of the proposed check dam in the gully near Nanyangapokoy.



Figure 30. Cross-section A approximately 30 m downstream of dam wall





--- Cross-section dam wall

Figure 31. Cross-section B at check dam wall site



Figure 32. Cross-section C approximately 55 m upstream of dam wall





--- Cross-section inflow north

Figure 33. Cross-section D at the northern inlet, approximately 65 m upstream of dam wall

The gully sides consist of fine graded material (silt) with occasional intercalations of coarser river sediments (sand, gravel and boulders in layers) and are vulnerable to erosion. It is very important to design a spillway with correct size and anchor the check dam with side wings dug into the gully walls. There are no villages downstream of the proposed dam site, and the gully system evolves to a river that converges with the main river approximately 3,5 km downstream. More detailed calculations of spillway size must be done prior to construction due to the erosion prone sidewalls of the gully. A rip-rap layer (erosion protection) of stones must be placed downstream of the check dam and spillway to prevent failure due to erosion at the dam toe. These more detailed calculations are not within the scope of the current assignment.

A simple estimation of storage volume in the check dam is 1200-1400 m³ if the dam wall is built 2.4 m high to +702 m.a.s.l. Check dams can be built by filling sandbags with silt and dirt. The existing material in the gully bottom + sides should be excavated to increase storage volume and can be used to fill the sandbags. The check dam could provide water for livestock and nearby fields for several months after a normal rainy season thus decreasing the pressure on other water sources and saving them for the drier period.

Some infiltration through the gully bed will probably occur. To take advantage of this a well can be dug on the surrounding plateau a few meters from the gully downstream of the dam wall.

2.4 Lotimor village

The roof of the school in Lotimor is very suitable for rainwater harvesting. With the addition of gutters and a storage tank to lead the harvested water to, this could be a very good addition to the water supply of the community (see general principle in Figure 34). The water harvested could be used by the school children as well as the teachers and reduce the pressure on the nearby borehole.

For the school in Lotimor (area of 270 m²) the total collected amount is estimated to be between 70-140 m³ (based on assumed yearly rainfall between 300-600 mm).

Mm rainfall/year*area of roof*efficiency (tin roofs has a high efficiency of 90%)=0.3*270*0.9= 72 m³





Figure 34. The general principle of rainwater harvesting from rooftops and the use of separator and filtering mechanisms to treat the water. (Oduor A.R. Gadain, H. M. 2007)

Lotimor village has four boreholes, two of these are functioning. BH1 by the school has slightly saline water while BH4 at the old Catholic mission station has fresh water. There is no information on the depths of the two boreholes that provide information on the reason for this, but a qualified guess is that BH1 is deeper and penetrates rock with salt bearing minerals (e.g. halite) or older groundwater that has been subject to long-term ion exchange and mineral enrichment by weathering of minerals. See Table 1 and Table 2.

2.5 Riverbed Lotimor

The project team has assessed alternative water resources in Lotimor valley. The project team assessed parts of the riverbed around Lotimor to evaluate the prospects of sand dams, sub-surface dams, dug wells and hafirs, see Figure 35 and Figure 40.

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Figure 35. Surveyed areas west of Lotimor village



Figure 36. Scoop hole 5 m deep, 4,70 m depth to static water level southwest of Lotimor village.

In the area southwest of Lotimor village, the villagers have dug several scoop holes in the riverbed. One of those reached the groundwater and was used for watering livestock and for human consumption (Figure 36). After each flood event the hole collapses and needs to be dug again. Considering the presence of layers of gravel and boulder in the river wall adjacent to the scoop hole, it should be possible to dig out a well on the side of the river that reaches the local aquifer, a location that would be much safer to damages from floods in comparison to the present one. The river sides are relatively high beside the scoop hole (4 m approximately), and digging a well involves more work than digging in the riverbed itself. However, the long-term benefits are huge as it can serve for several years without needing to be redug after each flood. A dug well should be constructed with casted concrete well rings. A hand pump helps protect the water from contamination of buckets etc., but an opening for buckets should be made so the well can be used when the pump is not functioning.

The project team assessed the feasibility of sand dams in the river west and south-west of Lotimor. Part of the riverbed is covered by medium to coarse sand, while other parts contain more silt. Three areas are marked as potential sites in Figure 35. The slope of the riverbed was measured for the site downstream of the scoop hole and was found to be approximately 0.1% which is low and can increase risk of deposition of silt and mud in an eventual sand dam.



Figure 37 Slope of riverbed downstream waterhole west of Lotimor

Approximately 1300 m north of Lotimor village a basalt dyke outcrops at two locations and cuts off the riverbed. This creates a natural sub-surface dam, see Figure 38 and Figure 40.



Figure 38 Basalt dyke outcropping and cutting off groundwater flow in riverbed. Arrows indicate basalt rock outcrops

The slope of the upstream riverbed is low (approximately 0.4%) which means that there are risks for deposition of silt in a sand dam or dam (Figure 39). Also, the river sidewalls are low and during high flows the river floods the adjacent low-lying river plain. This implies that the site is not suitable for sand dams.



Figure 39. Slope of riverbed upstream of basalt dyke south of Nakore village

A hafir or could be built on the western or eastern side of the river and be recharged through a channel from the river during flow events.

The area upstream of the basalt dykes has a high groundwater potential due to the formation of a natural sub-surface dam. Shallow water holes were observed with moist soil at relatively small depths (approximately 1 m) compared to downstream areas of the dyke. Another indication of higher groundwater table upstream of the basalt dyke is a field with crops that seemed to do well in spite of the drought and the presence of moist soil when digging nearby the fields. All this indicates a higher groundwater table compared to the area downstream of the dyke.



Figure 40. Detail site surveys north of Lotimor village

It is recommended to dig wells close to the river, but on side of the riverbank upstream of the rock outcrops where the groundwater table is relatively high.



3 Field assessment - Upper Plateau

The upper plateau with its inaccessible position and limited boreholes would do good from a more varied supply of water from multiple sources to reduce the pressure on the few functioning boreholes in the area. The population rely on boreholes for water supply to a large extent as well as scoop holes in sandy riverbeds located further from the edge of the plateau. There are three hafirs constructed by the local community that are good examples that could be replicated. These are located close to the edge of the plateau where other water supply options are limited. The following sections describe the more detailed findings from the area on Upper Plateau:

3.1 Lokengot

The village of Lokengot has two hafirs nearby. These have been constructed over several years where the owner of the hafirs allows community members to get water in exchange for their assistance to dig the hafir deeper. The hafirs were situated in a sloping landscape where small canals have been dug upstream to divert water into the hafir. These are quite limited and could be expanded to allow increased inflow to the hafir. The soil that has been dug out from the hafir by the community is used to increase the height and strengthen the walls surrounding the hafir. The initiative to construct the hafirs have come from the community themselves, which is why this is a great to technique to build further on (Figure 41).

Available source(s) of water and associated technique(s)

Hafir

Seasonal scoop holes in riverbeds (in general limited to areas located > 3000 m from Lokengot

General water supply situation at the time of the assessment:

Ok: water is still available in the hafirs but when that water runs dry the community needs to travel down to Nanyangachor for water (a large portion of the community will also migrate with the cattle in that case).

Potential improvements?

Dig the hafir deeper, to increase storage capacity and decrease evaporation losses

Construct more hafirs

Dig the upstream canals deeper and extend the network to collect more water (for Hafirs)

Addition of silt traps before water enters the hafir

Construct birkads in connection to the hafirs (see general description of technique above)

Shallow wells dug to the bedrock (the soil layer is generally thin on the plateau) downstream of the Hafir can collect some of the water that infiltrates from the Hafirs.

Sand dams in the Nayionangor area, approx. 3-4000 m north-east of Lokengot village



Figure 41. A fully functional hafir outside the village of Lokengot.

3.2 Nakedengoro

The hafir in Nekedengoro is of the same type as the ones found in Lokengot but this one had already dried out when the team visited the site on 2023-01-28. The general idea of construction was also similar to the above-mentioned hafirs.

Available source(s) of water and associated technique(s)

Hafir

Dug-out scoop holes (not close to the village though)

General water supply situation at the time of the assessment:

Ok: water is still available in the hafirs in neighbouring Lokengot but when that water runs dry the community needs to travel down to Nanyangachor for water (a large portion of the community will also migrate with the cattle in that case).

Potential improvements?

Dig the hafir deeper

Construct more hafirs

Dig the upstream canals deeper and extend the network to collect more water

Addition of silt traps before water enters the hafir

Construct birkads in connection to the hafirs (see general description of technique above)

3.2.1 Reconnaissance Lokengot/Nakedengoro/Nayionangor area

Due to the proximity to the water divide close to the edge of the plateau, the Lokengot and Nakedengoro villages have no streams. Sweco had, as part of the desk-based initial parts of the study, identified interesting sites for potential sand dams using remote sensing technology, and some of these were visited (see Figure 13).

In the village of Nayionangor there is a borehole (currently non-functioning due to pump failure) and a potential for a small sand dam in the stream where outcropping bedrock creates a natural barrier in the stream. The stream has a relatively small catchment and the width of the riverbed is only 5-8 m. The material in the riverbed consists of stones, coarse sand and gravel and is eroded to the bedrock in many places. There is potential for a small sand dam downstream of the borehole (area A). A rapid survey of the riverbed profile and cross-section was made here.

Further downstream after the junction of two streams, the width of the riverbed increases to 10-15 m and there are three separate areas with coarse sand and gravel that could be potential sites for sand dams (site B). There are outcrops of bedrock that cuts off the stream at three sites that could be potential sites for sand dams. A disadvantage of site B is that the river sidewalls are rather low in this area and a sand dam wall needs to be wide and the resulting sand and groundwater reservoir will be thin at the sides with high water losses to evapotranspiration as a result. Unfortunately, there was no time to survey the riverbed slope and cross-section at these sites (B) on this short mission. It is recommended to perform a survey of area B as the potential for storage probably is higher than in area A. Three test pits were dug to 0,8-1,15 m and showed coarse sand and gravel. No groundwater table was found, but the soil was moist. The villagers had been digging scoop holes but they had dried out at the time of visit. The riverbed sediments are thin at places with outcropping bedrock. See Figure 42.



Figure 42. Riverbed at site B in Nayionangor after the junction of the streams

3.2.1.1 Site survey at Nayionangor sand dam site A

This site has a width of the riverbed of approximately 6-8 m and compared to most stretches of the stream a bit steeper river sides. There is outcropping rock that cuts off the riverbed and is a suitable site for a dam wall. It is not an optimal site for a sand wall due to the low angle of the sides resulting in a long and low dam wall, but the near distance to the Nayionangor borehole means that it can be complementing this during some months after the rainy season thus reducing the pressure on the borehole and aquifer.

A test pit was dug to 0,8 m where weathered bedrock was encountered. According to the locals the site was used for scoop holes after the rainy season. A soil sample was analysed, and the porosity was found to be 0,25 which is high. The soil did not contain any silt or clay.

One cross section was measured at the site of the proposed sand dam wall, see Figure 46



Figure 43. Rock outcrop suitable for sand dam wall, Nayionangor site A



Figure 44. Test pit at Nayionangor site A





Figure 45. Profile of the riverbed at Nayionangor site A measured from the foot of the proposed sand dam wall, Nayionangor site A



Figure 46. Cross-section of valley at dam wall site, Nayionangor site A

3.2.1.2 Conceptual design ideas of sand dam at Nayionangor site A

A potential sand dam at Nayionangor would be small in size but could potentially benefit the local community. The foundation of the dam would be placed on the rock outcrop that can be seen in Figure 43. It is not recommended that the dam height would exceed 1 m since a higher dam would result in a very wide dam as well as be more costly. Figure 47 shows the potential amount of sand accumulation (level and volume) with a 1-meter-high dam at the site assessed. The storage of water amounts to approx. 165-170 m³ calculated with an effective porosity of 0,25 in the sand material.



Figure 47. Profile of the riverbed at Nayionangor site A with indications of level of potential sand accumulation upstream (168 m³ of water can be stored in the sand dam).

3.3 Kaloreng

The village has a borehole nearby with a generally good supply of water. However, many of the boreholes on the plateau have either not been functioning or have dried out (3 out of 7 are not working) so there is still a need to strengthen the general water supply on the water plateau to save the borehole water for times when all other sources of water have dried out. There is a riverbed not far from the village where the team assessed the possibility of constructing sand dams. The team found a number of suitable spots and did a detailed assessment of one of them (a site where the local community have been digging for water and where water was still available at the time of the visit by the team).

Available source(s) of water and associated technique(s)

Borehole

Dug-out wells in nearby riverbeds

General water supply situation at the time of the assessment:

Ok-Good: water is still available from dug-out wells (used mainly for cattle now) and the domestic water use is taken from the borehole. However, as mentioned above, the water supply situation needs to be strengthened to save the borehole water for more challenging times.

Potential improvements?

Construct hafirs (based on the examples of Lokengot and Nakedengoro

Construct birkads in connection to the hafirs (see general description of the technique above)

Construct a sand dam in the nearby riverbed (see general description of the technique above)

3.3.1 Reconnaissance Kaloreng area

The Kaloreng area is dependent on one borehole for current water supply. The borehole is sited adjacent to a stream. The project team has surveyed possibilities for water harvesting downstream of the borehole.



Approximately 200-500 m downstream of the borehole there are a few sites with outcropping bedrock that creates natural barriers in the groundwater flow along the river (area A), see map in Figure 13. The material in the riverbed consists of coarse sand and gravel with no silt content. The width of the stream is limited to approx. 5-7 m. Test pits were dug to 0.8 m depth, and no groundwater was found. According to the local elders, there is water available after the rainy season. Some sections of the riverbed consist of bedrock. The height of the river sides is low, approximately 0.5-1 m, and the river regularly overflows its natural course. The stream forms several forks. The low river walls are the main limiting factor to implementation of sand dams in this part of the river.

Area B is located approximately 2200 m northeast of Kaloreng (Figure 13).

In area B the river channel has eroded rather deep into the bedrock (basalt) with steep rock sidewalls and several natural rock steps outcropping in the riverbed. The material in the riverbed consists of coarse sand and gravel. A scoop hole was used for water supply. This area is suitable for a sand dam, and a more detailed survey was made by the project team, see further details below.

Area C is located approximately 600 m downstream from site B and has some basalt outcrops forming natural barriers. The riverbed is eroded into the topsoil (silt) and has vertical sides. Some stretches have river walls of limestone on the southern side of the river, see Figure 48 and Figure 50.



Figure 48. River wall limestone Kaloreng site B



Figure 50. Water hole dug into limestone. Note the vertical sides of soft topsoil of the riverbed behind.



Figure 50. Soil profile in scoop hole, Kaloreng site B

Several water holes were dug into the riverbed as well as into the underlying limestone rock, see Figure 50. This shows that the limestone is not impermeable and that water from the riverbed can infiltrate and form local aquifers with very limited areal extent in the fractured upper parts of the limestone. From a sand dam perspective, it is preferable with impermeable bottom for easy access to the stored water. The riverbed elevation profile is relatively flat, and a sand dam could potentially store a large volume of water. Due to the sidewalls of relatively soft topsoil, however, there are risks of erosion on the sides of a dam wall which could result in a collapse of the river sides. This can be mitigated using proper anchoring of the sand dam walls and proper design of spillways, but as Across has no previous experience of constructing sand dams, area B should be prioritised as this involves less risks.

3.3.1.1 Survey Kaloreng site B

The material in the riverbed consists mainly of coarse sand and gravel, and a scoop hole had been dug to 1.4 m and was used for water supply, see Figure 50. The porosity of the sand and gravel at 0.5 m depth in the scoop hole was examined and found to be 0.26. No silt or clay was found in the test pits.

There are several outcropping rock steps in the riverbed at site B, and the stream has eroded into the bedrock with steep rocky sidewalls. There is a rock step with minimum width of approximately 2.2 m that would be suitable as foundation for a sand dam wall. There is another rock step of approximately 2 m height at 40 m distance from the proposed dam wall, see profile for the riverbed in Figure 51.





Figure 51. Profile of the riverbed at Kaloreng site B measured from the foot of the proposed sand dam wall



Figure 52. Cross-section dam wall, West-East





Figure 53. Cross-section 20 m upstream from dam wall, West-East



Figure 54. Cross-section 40 m upstream from dam wall, West-East





Figure 55. Cross-section 100 m upstream from dam wall, West-East

3.3.1.2 Conceptual design ideas of sand dam at Kaloreng site B

Sweco proposes that a sand dam should be constructed in stages of 1+1 meters, the height could eventually be increased to up to 3.5 meters if the initial stages will be deemed successful. Figure 56 shows potential dam wall heights at the dam wall cross section. Figure 57 shows a conceptual sketch of the dam in profile and accumulated sand behind the dam wall. Table 8 shows the potential accumulated storage volume with different heights of the dam. Sweco recommends that a dam wall of 3.5 m height is constructed, this could have a storage of 1100-1200 m³ of water. This volume could supply 1000 persons with 10 litres per day for 120 days. Access to the water could be through collector pipes and a distribution point downstream of the dam. However, as the whole sand dam would drain if a valve broke due to malfunction, damage of floods or vandalism, Sweco recommends that the water is accessed from the upstream side of the dam wall. This would ideally be done through collector pipes in the sand dam connected to a collector well at the side to allow installation of a hand pump or bucket system, thus reducing risks of contamination from scoop holes and animals accessing the sand dam surface. However, the sloping rock walls complicates construction of collector well. To avoid risks of collapsing walls of scoop holes, two-three wells with concrete well rings can be dug into the sand dam and protected with e.g. gabions from the flood events. There is a risk that the wells will be filled with sand, these can be dug out and cleaned by hand. It is laboursome but common in other parts of the Horn of Africa region.





Figure 56 Section of the river at the proposed dam site with indications of sand dam wall heights



Figure 57. Conceptual sketch of the initial stage of a sand dam at the Kaloreng site (the dam height in the picture is around 1,5 m). Planned final total dam height is 3,5 m.



Figure 58. Profile of the riverbed at Kaloreng site B with indications of level of potential sand accumulation.

Table 8 Storage volume for different dam wall heights, Kaloreng sand dam. Calculated with measured drainable porosity of the sand = 0.25.

Sand dam wall height (m)	Elevation (m.a.s.l)	Storage volume of water (m ³)
2	1047	280
3	1048	873
3.5	1048.5	1130

It is recommended that the more detailed dam design follows the guidelines developed by Madrell and Neal in 2012 with clear instructions on the design of the dam when it comes to the handling of erosion to avoid dam failure, design of different spillways (Figure 59) and thickness of the dam in relation to the height (Figure 60). Many sources recommends that the sand dam is built in stages to allow a gradual filing of sand. Recommended stages in Kaloreng could be: year 1 - 1,5 m, year 2 - 2,5 m and year 3 - 3.5 m. A stepwise construction would also allow PMU and Across to evaluate the quality of the material and craftmanship and see if adjustments are needed. It is also necessary to evaluate the dam safety situation continuously. There were no permanent risk objects observed directly downstream (around 1 km) of the dam site at the time of the assessment even though the team met with people who were digging scoop holes to access groundwater. This activity is limited to the dry season and the risk of dam failure is highest when water is flowing in the river during the rainy season. With this in mind, together with the limited height of the dam and the fact that it mainly stores sand (a failure would mainly form a cone of sand directly downstream of the dam, the added water flow from the dam would probably be negligible in comparison to the water that is flowing in the river naturally), makes the risk of any impacts in the case of a dam failure very low.



Figure 59. The width and position of the first flood spillway (Maddrell, S., Neal, I., 2012).



Figure 60. Relation between dam width and height (Maddrell, S., Neal, I., 2012).



4 Field assessment – Nanyangachor

A short survey was also conducted upstream of Nanyangachor (see Figure 13) where a potential subsurface dam site was identified. The survey was not fully completed due to resistance to any interventions by the local community leaders, Across' staff assessed the situation to be too hostile and decided to stop the survey in this particular area. Before the survey was stopped, it was assessed that the site had deep layers of coarse sand material suitable for groundwater storage, so a collector well could be suitable to construct next to the river. There were a number of scoop holes at the site of which one of them still had water available.



Figure 61. Overview of site survey in Nanyangachor.



5 Recommendations

This section provides a set of recommendations by the Sweco team to guide PMU's and Across' continued work on strengthening the water supply in Lotimor and Upper plateau. The first section is a list of general recommendations that should guide future interventions in general while the second section is a specific list of sites assessed that should be prioritized for a pilot project as a first step for a wider engagement for the improvement of water supply and reversal of land degradation in the Nanyangachor, Upper plateau and Lotimor areas. The pilot projects should be seen as both directly beneficial for the communities, the environment and as a steppingstone for future joint capacity building interventions by PMU and Across in South Sudan.

5.1 General recommendations

- To be successful, boreholes must be drilled in areas with potential for a large catchment as well
 as geological structures. Before procuring additional boreholes from a drilling company,
 consider consulting a specialist hydrogeologist to make geophysical surveys based on a
 conceptual understanding of the groundwater in the area and not primarily based on close
 access to the villages. This to allow for siting of boreholes at the optimal locations to provide a
 high yield and a large catchment to decrease the vulnerability to groundwater depletion during
 droughts
- Several boreholes have the pump intake above the main water strike, and the borehole certificates indicate that pump installation depth often is on average 30 m above the bottom of the boreholes. The volume below the pump inlet cannot be accessed, and it is possible that the groundwater level and the main water strike is roughly at the same level. All the boreholes have casing in PVC all the way to the bottom and it is therefore not a risk to install the pump below the main water strike or close to the bottom of the borehole. This could provide more water in some of the boreholes that are seemingly dry. Sweco recommends that the pump intakes are installed below the main water strike and as deep as possible in the boreholes allowing for a larger storage in the borehole itself.
- Advocate for conjunctive use and management of water resources to maximise the yield and minimise losses. Different water resources can be used in different seasons to decrease the pressure on the boreholes until periods of drought or when other sources have dried out. Different sources can also be used for different purposes, e.g. hafirs for livestock and irrigation and groundwater for human consumption,
- Sweco also recommends Across and PMU to consider introducing casting of concrete well rings. The well rings protect the current water holes from collapsing and with techniques to dig inside the well rings, they can reach much deeper allowing for more secure access to groundwater.
- Dig wells nearby existing water holes in the riverbed but on the riverside to protect it from floods. With well rings the wells can be dug deeper, securing better access to groundwater, and the wells can be equipped with a hand pump, rope pump or a rope and bucket system.
- Build hafirs recharged by surface flow nearby Zai-pit demonstration plots and use water for irrigation
- Close to the edge of the upper plateau, the catchment areas are small and the conditions for boreholes or dug wells are not good with high risk of failure. Hafirs and birkads that collect water from surface flow are recommended interventions. Birkads can be constructed with roofs to decrease evaporation losses.
- Land degradation is a major concern in the project area due to overgrazing. Especially the fertile brown soft soil rich in organic material is vulnerable to erosion and should be protected. Thus, it is a general recommendation to construct Zaï pits (as already introduced in the ongoing Across/PMU project) and half-moons to allow water to infiltrate more easily into the ground.



This is a good example of nature-based solutions (NBS) to increase infiltration capacity and to revert land degradation in arid areas (and the above-described issue of reduced soil moisture in the area, see section 1.7.4). It is recommended that the construction of Zaï pits is combined with the construction of half-moon pits and hafirs to both reduce soil erosion, increase infiltration of water over larger areas and making water available for farming for an extended period of the year. Sweco recommends that introduction of Nature-Based Solutions such as earth bunds should be integrated with awareness raising and training of local communities on land and water management with regards to e.g. risks of over-grazing and the importance of vegetation on reducing erosion.

• Across and PMU should collect and save all borehole certificates and keep them in the project file. They contain important information on the boreholes and are a support when assessing optimal depths for installation of pumps etc.

Priority	Technique	Description (section)	Area
1	Sand dam	3.3.1.2	Kaloreng
2	Birkad recharged by river	2.2.1	Nakoré
3	Sub-surface dam	2.1.1	Lotuko
4	Introduce casted concrete well rings		
5	Hafirs	Build hafirs recharged by surface flow nearby Zai-pit demonstration plots	Upper Plateau
6	Sand dam	3.2.1.2	Nayionangor
7	Hafir and earth bunds	2.1.2	Lotuko

5.2 Recommended pilot interventions

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The Republic of Sudan Government of Southern Sudan Ministry of Water Resources & Irrigation Directorate of Rural Water Supply and Sanitation **BOREHOLE COMPLETION RECORD** PROJECT BRILLING OF ONE HAND JOUMP BOREHOLE COMPLETED WITH INSTALLATION CONTRACTOR GREAT NILE BRILLING COLFUNDING SOURCE PMU. IMPLEMENTED BY ACROUS(SSD). ORG Sketch map Location 20 State FASTERN FOULATORIABorehole Nº 05 County KAPVETA FAST Long. E 35 5'41.86" Payam LOTIMOR monntain Boma NAKUBOCHA Lat N 05° 34' 25.38" Village NAMUNYOGOR Elevation 731M Site NAMUNIYDGOR Borchole ID Use Community water supply Health facility Domestic water supply Education facility eason. Community center Test well] Private compound River Property or handed over to ACROSS (38) · ORG. Sitting Deophysics Vertical Lectrical Sormeling. horimore Center Other: Sevinna. Approximate scale : Drilling consumption Drilling data Start date 24 09 2020 End date 25 09 2020 Diesel......[Lt] Total depth 50.0 [m] SWL 13.70 Engine Oil......[Lt] Main water strike .23...[m] Yield 3 [milting Dynamic water level 36. [m] **Drilling** operation Drilling diameter inch mm mm @ 152.4 From O.O [m] To 50 [m] Method Hr KD fary Ø..... From [m] To [m] Method Method of drilling Percussion Hand-drilled M Air rotary *Mud rotary* DTH Rig make KD

UCCESSIFULL SITE IS KM from SITE 4 and 10 Km from LOTIMOR-C.

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s Water quality	T°	ncfu per 100 ml cfu per 100 ml

the p

PUMP TEST REPORT 05 Agency / Contractor: CROSS Corputnile S. C. Borehole no .: Faleon Location: Manningogor Submersible pump: Site: Pump depth [m]: 40.00 RICHTARD Static water level [m]: 13.70 Operator: Starting test time: 25-10-912020 Date: 7=10 am Time [hh:mm] Water Drawdown [m] Yield Remarks Recovery Lever[m] [l/min] [m] 36.00 00:00 13.40 0.00 14.54 0.84 00:01 34.86 00:02 15.31 1.61 33.72 2.38 00:03 6.08 32.58 00:04 16.85 3.15 31.44 Clear discharge. 3 amilt 17.62 30.30 00:05 3.92 18.39 4-69 00:06 19.16 5-46 28.02 00:07 26.88 00:08 19.93 6.23 25.74 7.00 20.40 00:09 24.60 21-47 7.72 00:10 23.46 22.24 8.54 00:15 23-01 22.32 00:20 9.31 23.78 21.18 00:25 10.0% 3.omilt clenr 20.04 24.55 00:30 10.781 25-32 18.90 00:35 11.62 26.09 17.76 00:40 12:39 26.86 00:45 13.16 16.62 27.63 13-93 15-48 00:50 14.34 28.40 14-70 00:55 3 Om MA clear. 29.17 he 01:00 15.47 4.26 29.94 01:10 16.24 = 85.51% 30.71 17.01 01:20 31.48 17.78 01:30 32.25 01:40 18.55 33.02 01:50 19-32 8-Om SHA 33.79 s Change. 20.09 0 in -0 02:00 34.51 02:15 20.86 Pump test executed by: 35-33 21.63 02:30 Great Nile Iniling 36.00 22.30 02:45 3 owith 36.00 22.30 03:00 03:15 schange Ahupti 03:30 03:45 04:00

25/09/2020 Borehole completion date was hiclessionly Completed fully with e Borel Comments 8 plat "Instal tion a

10

		Borehole Log and Construction Details			Constructions	Scale
rom	То	Lithology	Thik Ness	ОМ	and the state of the state of	SIH TOP CuP
)-()	4-0	Black/gray lop loanny soil		2- 4- 6-		x ~ ^ x x x x x GL '
		with some groupish weather grown ter and dry fractured	yeks.	8+ 10- 12-		-Upvc plain Casings.
		Groupsh Course gramed frac day dycks with some Coarsa Graynsh Coarse growned quantz	nd.	14- 16- 18-		-Gravel pack
		Yellowish brown Coarse gra weathered guartailes with	· · /	20- 22- 24-		-UPVC Scree
2=0	50-0	Some Slack Clay. Grayish fine grained guantz-	divites	26- 28- 30-		Casnings
		with some greenish weather	red	32- 34- 36 -	1 2 2	-UPVC Ple Casings
		0		38-		-152.4mm
				Un- Ult- Ult-		Hole
8				618- 50-	and the second	-50.0m
						-50.0m drillev der Britom pl
1.4						

BOREHOLE COMPLETION CERTIFICATE BE SIGNED BY: LOCAL AUTHORITY FOR THE EMPLOYER FOR THE CONTRACTORS Company Name: Organization Name: Authorities: A CROSS-SSM. ORG Signatory: WASH Accistant Q GREAT NILE & CO. 1.70 Signatory: Signatory Officer 500 Date: Date: Date: 9 2 09 D 2020 020 10 Signature: Signature: Signature: BRILL Stamp: Stamp: Stamp P.O.Box 132 JUBA- SOUTH SUDAN Annex 1

SUCCESSIFULL SITE 24 Km from Nonyoungachor Center.



The Republic of Sudan

Government of Southern Sudan Ministry of Water Resources & Irrigation

Directorate of Rural Water Supply and Sanitation



BOREHOLE COMPLETION RECORD

PROJECT DRILLING OF ONE HAND PUMP BOREHOLE; COMPLET WITH INSTALLATION. CONTRACTOR GREAT NULE DRILLING CO. LEDFUNDING SOURCE P.M.U. (IMPLEMENTED BY ACROSS (SSd). Drg)

i Borehole ID	Location State ERSTERN FLAUATORIABorehole N° 91 County KAPDETA ERST Payam NANYAACACHORLong. E 34°53'40.14 Boma NAMULOKONYIT Lat. N 05° 30'54.00 Village KAUTO PLATERUElevation 1067 M' Site KAUTO PLATERUE Use Site KAUTO PLATERU Use Community water supply Health facility Domestic water supply Education facility Community center Etwell Private compound Test well Property or handed over to ACROSS SSN ORG Sitting Vertical Lectical Sound	."" #" 10	LORIND	TO PEKIM A AA A AA A AA A	from yuchor.
1.0	Other: DeVining.	U Appro	oximate scale :	Vot to scale.	
é Erilling operation	Drilling data Start date 2108/2020 Total depth Start.0.[m] Total depth Start.0.[m] Main water strike S[m] SWL AHL.0.[m] Main water strike S[m] SWL AHL.0.[m] Dynamic water level S[m] Yield 2.13 Drilling diameter inch Main Inch Method Anr.h.0.ary Start Image: Start level Drilling diameter inch Main To SH:0m Method Ann Method Anr.h.0.ary Start Image: Start level Image: Start level Image: Start	Drilling consumption Diesel Engine Oil Hydraulic Oil Hammer Oil Foam/polymer	[Lt] [Lt] [Lt] [Lt]		

- 	Casing type	Filter pack (gravel pack)
	\overrightarrow{V} uPVC	Composition Gravel Source River
uo	Threaded	Units 🗹 bags [40 kg] 🗹 kg 🗌
Borehole construction	Bottom plug Height above/below ground level. Q. 5	[m Amount used 30 5aps Depth to top 0.00 [m]
resta	Plain casing & Screen installation inch	Grouting
le co	mm 101.6 Type P From 0.0 (m) To 58.0 (m) 0.101.6 Type 5 From 58.0 (m) To 63.0 (m)	\Box ves \Box no \Box <u>Cement</u> \Box <u>M</u> ikolit \Box
eho.	\emptyset 101.6 Type P From $63^{\circ}0$ [m] To $66^{\circ}0$ [m] Slot.	Type From [m] To [m] Amount
Boi	@ 101.6 Type S From 66.0 [m] To 72.0 [m] Slot.	
	@ 101.6 Type P From 72.0 [m] To 75.0 [m] Slot.	
	Ø 101.6 Type S. From 75.0 [m] To 81.0 [m] Slot.	
	Ø 191:6 Type P From Slovim) To SURVIM	
		ackwashing 🔲 Jetting
ting		$arbid \ A \square \ Qther \dots \ arbid \ A \square \ Qther \dots \ Arbid \ A \square \ Arbid \ A \square \ Arbid \ $
tes	Comment the Borchale way	Catic Lactorilly demotope il
duun		Sar dircharad
Development & pump testing		J
ıent	Water level * H.a.g.l. = height above	1000 001000
udo	Measurement from $\mathfrak{O} : \mathfrak{O} : \mathfrak{O} : \mathfrak{O} : \mathfrak{O}$.	[m] Static water level (SWL). A. T. M. M. [m] Date A. M. O. A.
eve	Test pumping	
Q	Air-lift cap. Evaluation 🗌 Step Drawdown Test 🗌 🤇	
	Duration] Dynamic water level (final drawdown) $\bigcirc \bigcirc \bigcirc \bullet $. [m]
Pump & platform	Apron I Concrete slab Comment Lie Borehole was en	Date installed 22/08/2020 Depth of pump intake 60-0 [m] Type of pipes GI pipes Ø of pipes 144 Shicless'i fully Installed with IN12-X-deep Fitted around casing Drainage , Soak-away pit Fence I Computy Constructed with Vatio of 1224
	Physical quality	Bacteriological quality
	Color Taste Turbidity [M.	TU] Faecal coliformcfu per 100 ml
	T [°] [[°] C] TDS[mg/lt] CE	cm] E. coli totalcfu per 100 m!
~	Sample taken 🔲 Yes 🗌 No Date	Lab
\$	Comment	
quality	Comment	
ater quality	Disinfection	
Water quality	Disinfection Chemical used	Volume
Water quality	Disinfection	Volume
Water quality	Disinfection Chemical used	Distance

Local Site: Oper Date Date 00:00 00:01 00:02 00:03 00:04 00:05 00:06 00:07 00:08 00:07 00:08 00:09 00:10 00:15 00:20 00:25 00:30 00:35 00:40 00:45 00:55 01:00 01:10 01:20 01:30 01:50 02:00	rator: 2: 21	K	anto plute. Optomotor	all S	Pump depth [m]: Static water level [m]: Starting test time: Remarks	Hh	9m L. 9m Dam 1 Recovery [m] 60.00 59.37 58.74 57.22
Oper. Date. Date. Date. 00:00 00:01 00:02 00:03 00:04 00:05 00:06 00:07 00:08 00:09 00:10 00:25 00:30 00:40 00:55 00:40 00:45 00:55 01:00 01:20 01:30 01:40 01:50	rator: 2: 2:	Water Lever[m] 44.65 45.30 45.30 45.95 46.60 47.25 47.90 48.55 49.20 49.85	Drawdown [m] Drawdown [m] U. OD U. 65 I. 3U J. 95 2. 60 3. 25 3. 90 4. 55 5. 20	Yield [l/min]	Static water level [m]: Starting test time: Remarks	Hh	C.9M Down 1 Recovery [m] 60.00 59.37 58.74 58.74 58.11 57.48 56.85
Date. 00:00 00:01 00:02 00:03 00:04 00:05 00:06 00:07 00:08 00:09 00:10 00:25 00:30 00:45 00:55 01:40 01:20 01:20 01:30 01:40 01:50	2: 2:	Water Lever[m] 44.65 45.30 45.30 45.95 46.60 47.25 47.90 48.55 49.20 49.85	Drawdown [m] Drawdown [m] U. OD U. 65 I. 3U J. 95 2. 60 3. 25 3. 90 4. 55 5. 20	Yield [l/min]	Starting test time: Remarks		0 cam i Recovery [m] (9 0·00 5 9·37 5 8·74 5 8·11 5 7·49 5 6·85
Image Image 00:00 00:01 00:02 00:03 00:04 00:05 00:06 00:07 00:08 00:09 00:10 00:15 00:20 00:25 00:35 00:40 00:55 01:50 01:20 01:50 01:30 01:40 01:50 02:00		Water Lever[m] 44.65 45.30 45.95 45.95 45.95 45.95 47.90 47.90 48.55 49.20 49.85	Drawdown [m] 0.00 0.65 1.30 9.95 2.60 3.25 3.90 4.55 5.20	[l/min]	Remarks		Recovery [m] 60.00 59.37 58.74 58.74 58.11 57.49 56.85
00:00 00:01 00:02 00:03 00:04 00:05 00:06 00:07 00:08 00:09 00:10 00:25 00:30 00:45 00:55 01:00 01:10 01:20 01:30 01:40 01:50		Lever[m] 44.65 45.30 45.95 46.60 47.25 47.90 48.55 49.20 49.85	0.00 0.65 1-30 9.95 2.60 3.25 3.90 4.55 5.20	[l/min]			[m] 6 0.00 5 9.37 8 8.74 5 8.11 5 7.49 5 6.85
00:01 00:02 00:03 00:04 00:05 00:06 00:07 00:08 00:09 00:10 00:25 00:30 00:40 00:45 00:55 01:00 01:10 01:20 01:30 01:40 01:50		44.65 45.30 45.95 46.60 47.25 47.90 48.55 49.20 49.85	0.65 1.30 9.95 2.60 3.25 3.90 4.55 5.20		4 Clear discharge :		60.00 59.37 58.74 58.11 58.11 54.49 56.85
00:01 00:02 00:03 00:04 00:05 00:06 00:07 00:08 00:09 00:10 00:25 00:30 00:40 00:45 00:55 01:00 01:10 01:20 01:30 01:40 01:50		H4.65 45:30 45:95 46.60 47.25 47.90 47.90 48.55 49.20 49.85	0.65 1.30 9.95 2.60 3.25 3.90 4.55 5.20	2·13m]/	4 Clear discharge:		59.37 58.74 58.11 57.44 56.85
00:02 00:03 00:04 00:05 00:06 00:07 00:08 00:09 00:10 00:25 00:30 00:45 00:55 01:50 01:20 01:50 01:20 01:50 01:50		45.30 45-95 46.60 47.25 47.90 48.55 49.20 49.85	1-30 9.95 2-60 3.25 3.90 4-55 5.20	2.13m/	4 Clear discharge.		\$8,74 \$8,14 \$8,11 \$7,49 \$6,85
00:03 00:04 00:05 00:06 00:07 00:08 00:09 00:10 00:20 00:25 00:35 00:45 00:55 01:00 01:10 01:20 01:50 01:20 01:20 01:50 01:20		45-95 46.60 47.25 47.90 48.55 49.20 49.85	9:95 2.60 3.25 3.90 4.55 5.20	2.13m]	4 Clear discharge.		5 8-11 5 7.49 56.85
00:04 00:05 00:06 00:07 00:08 00:09 00:10 00:15 00:20 00:35 00:40 00:45 00:55 01:00 01:20 01:30 01:40 01:50 02:00		46.60 47.25 47.90 48.55 49.20 49.85	2-60 3.25 3.90 4-55 5.20	2.13m/	4 Clear discharge.		54.49
00:05 00:06 00:07 00:08 00:09 00:10 00:15 00:20 00:25 00:30 00:45 00:55 01:00 01:10 01:20 01:30 01:40 01:50 02:00		47-25 47.90 48.55 49.20 49.85	3.25 3.90 4.55 5.20	2.13m/	4 Clear discharge.		56.85
00:06 00:07 00:08 00:09 00:10 00:15 00:20 00:25 00:30 00:40 00:55 01:00 01:10 01:20 01:30 01:40 01:50 02:00		47.90 48.55 49.20 49.85	3,90 4,55 5.20	λ·[4 Oreal Mischarge		56.22
00:07 00:08 00:09 00:10 00:15 00:20 00:25 00:30 00:45 00:55 01:00 01:10 01:20 00:45 00:55 01:00 01:20 01:30 01:50 02:00		48.55 49.20 49.85	4.55				11 10 11 11 11 11 11 11
00:08 00:09 00:10 00:15 00:20 00:25 00:30 00:35 00:40 00:55 01:00 01:10 01:20 01:50 01:30 01:40 01:50 02:00		49.20 49.85	5-20				55.59
00:09 00:10 00:15 00:20 00:25 00:30 00:35 00:40 00:55 01:00 01:20 00:55 01:00 01:20 01:30 01:40 01:50		49.85				C. A. A.	54.96
00:10 00:15 00:20 00:25 00:30 00:35 00:40 00:45 00:55 01:00 01:20 01:30 01:50 01:50 02:00			2.84				54.33
00:15 00:20 00:25 00:30 00:35 00:40 00:45 00:50 00:55 01:00 01:20 01:30 01:50 01:50 02:00	11	50.30	P 1				5-2.70
00:20 00:25 00:30 00:35 00:40 00:45 00:50 00:55 01:00 01:10 01:20 01:30 01:40 01:50 02:00	1921 7 7	51 00	6-50				53.07
00:25 00:30 00:35 00:40 00:45 00:50 00:55 01:00 01:20 01:30 01:40 01:50 02:00	+	51.00	7.00				52.44
00:30 00:35 00:40 00:45 00:50 00:55 01:00 01:20 01:30 01:40 01:50		51.50	7.50				57.81
00:35 00:40 00:45 00:50 00:55 01:00 01:10 01:20 01:30 01:40 01:50 02:00	8 11	52.56	8.56	2.12m2/2	· Æden yjeld.		51.18
00:40 00:45 00:50 00:55 01:00 01:10 01:20 01:30 01:40 01:50 02:00		53.43	9.43	U SIIIIA			50.55
00:45 00:50 00:55 01:00 01:10 01:20 01:30 01:40 01:50 02:00		53.50	9:50				49.9-
00:50 00:55 01:00 01:10 01:20 01:30 01:40 01:50 02:00		54.00	10.00				49.20
00:55 01:00 01:10 01:20 01:30 01:40 01:50 02:00		54.57	10.50				48.6
01:00 01:10 01:20 01:30 01:40 01:50 02:00		33-36	11-36				48.0
01:10 01:20 01:30 01:40 01:50 02:00		55-50	11. 50	2-13/14	Clear discharge.		48.00
01:20 01:30 01:40 01:50 02:00	t. in	56.02	12 · D2		2		<u></u> A
01:30 01:40 01:50 02:00		36.52	12.5-2				0/R=75
01:50 02:00		57.01	13.01				B
02:00		57.50	13, 50				offer 1Ho
		57.99	13.99				
00 10		60.00	14:00				
02:15		60.00	14.00				
02:30		60.03	14.00			Pum	p test executed by:
02:45		60.00	14.00			Gre	sont Able In the
03:00		60.00	14.00.	2:13mill	- Cleur discharge c	Co	orhited -
03:15					6	i	
03:30							
03:45							

23 08/2020 Borehole completion date succession way Complet B Comments after a penod 20 Ule rea an or. SU P mering ap 0 e e Je orm

Borehole Log and Construction Details					Constructions Scale	
From	То	Lithology	Thik Ness	0M	-0.	sorehole Cap. 5m casing a.geh
0.0	40	Black top boil with reddish		5.		Gh.
		latentes and Grayish weathered		10-		
		Gramites en V Wayish weathered		15-		
4-0	8.0	Hellispers with Some few		20-		Gulm
		weathered greins.		25-	14 14 1	- Gravel Pac
3-0	<u>20 D</u>	Jellowish fine grained		32-	1	-152-4mm
		Su prollites with home few pebbles of grayish granitic greis		35-	122.4	drilled He
20-0	440	Grayich Course grained Course		40		201 201
5 		grained gramfic greiss with I lowe blank admoby bellite	1.	57-		-PVC Plan Casings.
4-0	52-0	Brownish Coarse grained		55-		Cosmys
2.0	60.0	Phellispers '		62.		- PVC Scree
	76.0	epoined quantzite - gravels;		65.		Casings.
		ducks with your greenish		70-		
760	84.0	Gravish Coarse granite rocks. Gravish Coarse grained gneiss.		75.		
		110033.		80 84.		- 84-0 m drilled depth
V					' R	ottom plu

* FOR THE CONTRACTORS	FOR THE EMPLOYER	LOCAL AUTHORITY
Company Name:	Organization Name:	Authorities:
GREAT NILE BRILLING CO. ETET	ACROSS-SSD. DRG	
Ciovactore	Signatory: WASH Assistant Officer.	Signatory:
Date: 23/08/2020	Date: 29/09/2020	Date:
Signature:	Signature:	Signature:
. Afrit 11	Trans	
Stamp:	Stamp:	Stamp:
ST ST	ACROSS	
	P.O.Box 132 JUBA- SOUTH SUDAN	
NY NEW MARK		

BOREHOLE COMPLETION CERTIFICATE BE SIGNED BY:
SUCCESSIFULL SITE 4Km from Site 1



The Republic of Sudan Government of Southern Sudan

Ministry of Water Resources & Irrigation

Directorate of Rural Water Supply and Sanitation



BOREHOLE COMPLETION RECORD

PROJECT GRILLING OF ONE HANS JUMP BOREHOLE COMPLETE WITH INSTALLATION CONTRACTOR GREAT NIKE BRILLING CONTRACTOR SOURCE PMU (IMPLEMENTED BY ACROSS (SIN)- ORG

Esteriole ID	Location State FASTERN FOUNTTRIBOREHOLE N° 02 County KAPDETA FAST Payam MAYANLACHTR Long. E 34° 51' 59.0" Boma LORIND Lat. N 05° 31' 33.0" Village LORIND Elevation 1133 M Site LORIND Elevation 1133 M Site LORIND Elevation 1133 M Site LORIND Elevation 1133 M Site LORIND Elevation 1133 M Property or handed over to ACROSS SD. OR Sitting Compound ACROSS SD. OR Sitting Compound Sleethlal S	SITE 2 4 Km from Site1	TO PEKIM TO Nermokohonyit TO Nermokohonyit TO Nermokohonyit TO Nermokohonyit
5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	Drilling data Start date 2.6.0.8.12.9.9 Fotal depth	Drilling consumption Diesel	

5 2009 - 200 - 200 - 200 - 200 - 200 - 200 - 200 - 200 - 200 - 200 - 200 - 200 - 200 - 200 - 200 - 200 - 200 - 200	24	
1 T 1-0	Casing type	Filter pack (gravel pack)
	$\overrightarrow{U} uPVC$ $\overrightarrow{V} Threaded$	Composition Gravel Source RIVER
tion		Units $[f_{bags}[.5], kg] [f_{kg}]$
e Borehole construction		[m Amount used
cons	Plain casing & Screen installation inch	Grouting
olec		yes no <u>C</u> ement <u>M</u> ikolit
reh		Type From
Bo	Ø. G. Type P. From 7.7. [m] To 82 [m] Slot	Type From
	Ø. U. Type S. From 82. [m] To 91. [m] Slot)	Type From
	O	Backfilling
,	Bevelopment P From 97 TO 100	
	Air-lift Over-pumping Surging Bac	ckwashing \Box .Jetting
ting		
p tes	Comment the Borcholo was lu	Clersi July developed Unhil
NU FYE	acteur yield was disci	
& 1		
tent	Water level * H.a.g.l. = height above gu	
Development & pump testing		[m] Static water level (SWL). U.O[m] Date 27/08/2
evel	Test pumping	
-	Air-lift cap. Evaluation Step Drawdown Test Co	
	Duration	$H_{\mathcal{T}}$ Dynamic water level (final drawdown)
511. GBN	Pump	
		Date installed 27/08/2020
	M IM2 x-deep Mono	Depth of pump intake
orm	Duba	Type of pipes
platform	Make 1M2 X-deep	Ø of pipes
વ્ય	Comment the Borchole was	encessionly constalled with 1
bumb	Well head and platform completion	X-deepa
đ	Pump stand 🗌 Welded on casing	itted around casing
		ainage 🛛 Soak-away pit 🗌 Fence
	Comment the Bare fale was	Successionly constructed
	with a ftan daved Constr	iction ratio of 1:2:4.
	Physical quality	Bacteriological quality
	Color Taste Turbidity [MTU	
	$T^{\circ} [^{\circ}C] TDS$	
lity	Sample taken Yes No Date	. Lab
Water quality	Comment	
ater	Disinfection	
Z	Chemical used	Volume
	Nearest sources of possible contamination	
	Type	Distance

Agency /	Contractor:		REATNILE D.C	eoLiBorehole no.:	02	
Location:		PRIKLD		Submersible pump:	Falci	m
Site:		1140		Pump depth [m]:	60.0	
Operator Date:	RICHA 27/08/	RD		Static water level [m]: Starting test time:	40-0 7:10 m	
Dale.	~11081	2020			7 :10 00	
Time [hh:mm]	Water Lever[m]	Drawdown [m]	Yield [l/min]	Remarks		Recovery [m]
00:00	40.0	0.00				54.00
00:01	40.48	0.48				53.42
00:02	40-96	0.96				52.84
00:03	41.44	1.44				52.26
00:04	41.92	1:92				3-1.68
00:05	42.40	2-40	3m?/Hr	Clear discharge		51.10
00:06	42.88	2.88		Ŭ		50.52
00:07	43.36	3136				49.92
00:08	43.84	3:84				49.36
00:09	44.32	4.32				48.78
00:10	44:80	4.80	3milla.	Clear discharge		48.20
00:15	45.28	5.28		J		47.62
00:20	45.76	5-076				47.04
00;25	46.24	6.24				46.46
00:30	46-72	6:72				45.88
00:35	47.20	7.20				45.30
00:40	47.68	7.68				44.72
00:45	48.16	8.16				44.14
00:50	48.64	8-64				43.56
00:55	49.12	9-12				43.18
01:00	49.60	9:60	3miltr	Cleur discharge.		43.00
01:10	50.08	10-08		U		
01:20	50.56	10-58			(Jage R=78
01:30	51.04	11.04				
01:40	51.52	11-52				yter 1Hr.
01:50	52.00	12.00				<u>J</u>
02;00	52.48	12.48	3milt	Clear discharge		
02:15	574.96	12.96		U		
02:30	53.44	13.44			Pump	test executed by:
02:45	53.92	13.92	3117		GRA	77 NILE BRILL
03:00	54.00	114-00	Smilt	Clear discharge.	CO.	hts .
03:15				U		
03:30						
03:45						
04:00						

. .

28/08/2020 Borehole completion date ۰. Complyted illess pull Q Deys Comments . fter a penarl of d for le n or read 0 One 200 form e ć D 1 nte

		Borehole Log and Construction Details			Constructions	Scale
From	То	Lithology	Thik Ness	0M	-0.5	STH CAP m-Casing age
0.0	4-0	Black top boil with		17- 20-	× 3X	GL'
• 4		Reddish brown Intentes and whitish weathered		30-		-Gravel
Y.D	8.01	1 1 2		50-		4" pvc pl
8.00	19.90	granntes with Norme granner Coarse grained griess Grayish Coarse grained	I	60- 70-		-4"PVC S
12-00		granastic gnéirs.		Po-		Casmys
)		Phellispers. Grayish Come grained		109		-100m
52-0	8D-1	granitic gneirs. Jellowish brown Course grained phellispers with son		-		dinile d deptk
89.Q	107.8	Ver meins.	×			Bottom Plug.
14						

FOR THE CONTRACTORS	FOR THE EMPLOYER	LOCAL AUTHORITY
Čompany Name:	Organization Name:	Authorities:
Great Nike Drilling Co. Etd	ACROSS-SSD. ORG	
Great Nike brilling Co. htd signatory: Gie Supervisor.	Signatory: WASH Assistant Officer.	Signatory:
Date: 28/08/2020	Date: 29/09/2020	Date:
Signature:	Signature:	Signature:
Almpani	mat	
Stamp: 5 South SUDAIL	Samp: ACROSS P.O.Box 132 JUBA- SOUTH SUDAN	Stamp:

BOREHOLE COMPLETION CERTIFICATE BE SIGNED BY:

SUCCESSIFULL SITE; 5KM FROM LOTIMOR. CENTER. AND 124KM FROM SITE 3.



The Republic of Sudan Government of Southern Sudan

Ministry of Water Resources & Irrigation

Directorate of Rural Water Supply and Sanitation



BOREHOLE COMPLETION RECORD

PROJECT BRILLING OF ONLE HANLS PUMP BOREHOLE COMPLETES WITH INSTALLATION. CONTRACTOR GREAT NILE BRILLING FUNDING SOURCE PMU. IMPLEMENTED BY ACROSS (SSD). ORG.

$\begin{array}{c} \text{General KAPDETA FAST} \\ \text{County, KAPDETA FAST} \\ \text{Payam } \mathbb{L} \text{OTIMOR} \\ \text{Boma } \mathbb{L} \text{OTIMOR} \\ \text{Boma } \mathbb{N} \text{AKOOREI} \\ \text{Isat } \mathbb{N} \text{ OS}^{\circ} 33' 9.53'' \\ \text{Village } \mathbb{N} \mathbb{A} \text{KOOREI} \\ \text{Isat } \mathbb{N} \text{ OS}^{\circ} 33' 9.53'' \\ \text{Village } \mathbb{N} \mathbb{A} \text{KOOREI} \\ \text{Elevation } \overline{760M} \\ \text{Site } \mathbb{N} \mathbb{A} \mathbb{K} \text{OOREI} \\ \text{Site } \mathbb{N} \mathbb{A} \mathbb{K} \text{OOREI} \\ \text{Isat } \mathbb{E} \mathbb{I} \\ \text{Domestic water supply} \\ \text{Ommunity water supply} \\ \text{Ommunity center} \\ \text{Private compound} \\ \text{Property or handed over to } \mathbb{A} \mathbb{C} \mathbb{R} \mathbb{O} \mathbb{S}^{\circ} \mathbb{S}^{\circ} \mathbb{S}^{\circ} \mathbb{O} \mathbb{R} \mathbb{G}^{\circ} \\ \text{Site } \mathbb{O} \mathbb{P}^{\circ} \mathbb{O} \\ \text{ORE } \\ \text{Substance of the supply} \\ \text{ORE } \\ O$	from NDR
County INIT DET AND Payam LOT IMOR Long, E $35^{\circ} 8'27.36''$ Boma MAKOOREI Lat. N $05^{\circ} 33' 9.53''$ Village MAKOOREI Elevation T60M Site NAKOOREI Use M Community water supply Health facility Domestic water supply Education facility Community center Test well Private compound Test well Property or handed over to ACROSS (SSD). ORG.	-
Village NAKOOREI Elevation 760M Site NAKOOREI Use Use Domestic water supply Health facility Domestic water supply Education facility Community center Private compound Property or handed over to ACROSS (SSD) • ORG - Site ORG - C'	-
Village NAKOOREI Elevation 760M Site NAKOOREI Use Use Domestic water supply Health facility Domestic water supply Education facility Community center Private compound Property or handed over to ACROSS (SSD) • ORG - Site ORG - C'	-
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Use Use Domestic water supply Domestic water supply Community center Private compound Property or handed over to ACROSS (SSA) · ORG-	
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Private compound Property or handed over to ACROSS [SS]. ORG.	IAL
Property or handed over to ACROSS (SSD). ORG.	2.
Citizen 2 2 2 2 1	
The second second and the second seco	20120
M Geophysics VERTICAL SLECTRICAL SOUNDINGS M Other: DEVINNING: Approximate scale: A (II) for the dialogue	nur
Other: DEVININING. Approximate scale: NJJ Lo SLING.	
Drilling consumption	
Start date 20/09/2020 End date 21/09/2020 Diesel	
Total depth 100^{-1} [m] SWL $946 \cdot 0$ [m] Engine Oil [Lt]	
Main water strike .6.8. [m] Yield	
Dynamic water level 7.8[m] Hammer Oil[Lt]	
Image: Second state of the state of th	
5 $Drilling diameter$ \Box inch $\Box mm$	
De D. 152.4 From O. O[m] To 1.00 [m] Method An Ritany.	
Ø From	
Ø, From [m] To [m] Method	
Method of drilling	
Percussion Hand-drilled	
Air rotary Mud rotary	
DTH Rig make. P.R.L	

s č Borehole construction	Casing typeFilter pack (gravel pack) \bigvee uPVCComposition $\square AV \in I : S.$ \bigvee ThreadedUnits \square bags [$\square R$] $\square R$ \bigvee Bottom plugHeight above/below ground level $0:5/189$ [mAmount used 2.3 \square Bottom plugHeight above/below ground level $0:5/189$ [mAmount used 2.3 \square Bottom plugHeight above/below ground level $0:5/189$ [mAmount used 2.3 \square Bottom plugHeight above/below ground level $0:5/189$ [mAmount used 2.3 \square Bottom plugHeight above/below ground level $0:5/189$ [mAmount used 2.3 \square Bottom plugHeight above/below ground level $0:5/189$ [mAmount used 2.3 \square Bottom plugHeight above/below ground level $0:5/189$ [mAmount used 2.3 \square Depth to top $Q:9$. [m] \square Bottom plugHeight above/below ground level $0:5/189$ [m \square mount used 2.3 \square Depth to top $Q:9$. [m] \square mount \square mount \square D101·bType \square From $0:0$ [m] \square mount \square D101·bType \square From $ [m]$ To \square mount \square D101·bType \square From $ [m]$ To \square mount \square D101·bType \square From $ [m]$ To \square mount \square D101·bType \square From $ [m]$ To \square mount \square D101·bType \square From $ [m]$ To \square mount \square D101·bType \square From $ [m]$ To \square mount \square D101·bType \square From $ [m]$ To \square mount <td< th=""></td<>
ë Development & pump testing	Development Image: Air-lift Over-pumping Surging Backwashing Jetting Duration. 1*0. [hr] Water: Limpid Turbid Other Comment Hie Borch Dle Turbid Other Comment Hie Borch Dle Turbid Other Static factors Hie Turbid Other Static level The Borch Dle Turbid Other Water level *H.a.g.l. = height above ground level Measurement from H.a.g.l* = .0:5. [m] Static water level (SWL)00. [m] Date .21/09/2.02 Test pumping Air-lift cap. Evaluation Step Drawdown Test Constant RateTest-CRT Short CRT Duration [hr] Discharge. 2: .0. [.M. Hr] Dynamic water level (final drawdown)
ë Pump & platform	Pump IM2 Afridev Submersible Date installed. 21/09/2020 IM2 x-deep Mono Depth of pump intake. 78.0 [m] Duba Type of pipes. GI PIPES. Make MATA Ø of pipes. IVu" Comment The Bore hale Sast Success for Users IVu" Well head and platform completion Fitted around casing Fitted around casing Fitted around casing Apron Concrete slab Drainage Soak-away pit Fence Comment Forehale Sast's factority Completed with Soak-away pit
č č Water quality	Physical quality Bacteriological quality Color Taste Turbidity [MTU] T° [°C] TDS [mg/lt] CE [µS/cm] Sample taken Yes No Date 24/04/2020 Lab Lab Comment No Date 24/04/2020 Lab Lab Disinfection Volume Distance Volume Type Distance Distance Distance Remarks MO MOM MARCA Mom Lamma Distance

Agency /	Contractor: K	CROSS/ COREM	NILE BRILLING	& Borehole no.:	04	
Location		PROVRET		Submersible pump: #	Falcon	
Site:		LOORET		Pump depth [m]:	4	30.00
Operator				Static water level [m]:		54.00
Date:	2110	9/2020		Starting test time:	7:00)am .
ime [hh:mm]	Water Lever[m]	Drawdown [m]	Yield [l/min]	Remarks		Recovery [m]
00:00	64.00	0.00				78.00
00:01	64.48	0.48				77.39
00:02	64.96	0-96				76:78
00:03	65.44	1-44				76.14
00:04	65-92	1:92		ara i citat anti		75.57
00:05	66.40	2.40	2.6m//4	Shiptly Clear		74.95
00:06	66.88	2.88		lischere.		74.34
00:07	67.36	3.36	y	Surge		73.73
00:08	67.84	3.84				73.12
00:00	68.32	4-32				72.57
00:10	(28.80	4.80				71.90
00:15	69.28	5-28				71.29
00:20	69.76	5.76				70.68
00:25	70.24	6.24				70.07
00:30	70,72	6.72	2.6m3/Hr	Clear dischane		69.46
00:35	71.20	7:20		<u>ceeur oursourine</u>		68.85
00:35	71.68	7.68		<u> </u>		68:24
00:45	72.16	8.16				67.63
00:50		8.64				67.02
00:55	72:64	9.12				66.41
01:00	73.12		9. br. 211	Clear discharge		66.32
01:00	73:60	9-60	aum	un urscharge		00'52
01:20	74.08	10.56		~		Of and Day
01:20	74.56					Jaye R= 83
01:30	75.04	11:04				alla 122
01:40	75.52	11.52				ingter 1772.
and the second se	76.00	12.00	2.6m21H	deur discharge		
02:00	76.48	12.48	L'OM ITT	New womange		
02:15	76.96	12.96		U	Dum	test executed by:
02:30	77.44	13.44				
02:45	77.92	13.92	2.6m314	alea distat	Grea	Antile drilling
03:00	78-00	14:00	a Gut Mr	Clear discharge.	_ 00,	hold :
03:15		4		U		
03:30						
03:45						
04:00						

22/09/2020 Borehole completion date Gem plated encless Joully was c -0 Bore on 0 P Comments . A Construction, non 22/09/2020 20 in cm on

		Borehole Log and Construction Details			Constructions Scale	
From	То	Lithology	Thik Ness	0М	BIH TOP O.SM Plan	n arg-h
0-0	8-0	Black top loanny soil with		10- 20-	Ghi	
<u>.</u>		Coarse gramed Coursend and oly douctured dycks		30- 40-	Gravel	'e ·
8-0	12-0	fractured dyeks		57- 69-	id i pack.	
12-0	29-0	grained quantzite gravels with		70- 80-	Screen PVC PL	
20-0	40.0	Jome Clay. Yellowish Coarse grained		90- 100-	Co sing	5,
400	480	Grayish fine graniel granite		110-	Clntled Botto	
48.0	56.1	Black Coarse gronned amphysollit with some few Shitish	es			
56-0 64-0			mles			
		with Some fractures at \$8m. Black/gray Coarse grained amphybollites.				
		10				

FOR THE CONTRACTORS	FOR THE EMPLOYER	LOCAL AUTHORITY
Company Name:	Organization Name:	Authorities:
GREAT NILE BRILLING CO.LTS	ACROSS-SUM. ORG	
Signatory: SITE SUPERVISOR.	Signatory: WASH Assurtant Officer.	Signatory:
Date: 22/09/2020	Date: 29/09/2020	Date:
Signature:	Signature:	Signature:
Amaderine	- Mark	
Stamp:	Stamp: ACROSS P.O.Box 132	Stamp:
······································	JUBA- SOUTH SUDAN	

BOREHOLE COMPLETION CERTIFICATE BE SIGNED BY:

SUCCESSIFULL Size; 19km from 2nd site.



Drilling operation

Ø.,

Drilling diameter

Method of drilling Percussion

Air rotary

DTH

M inch

O. B. From O.D. [m] Tolou. [m] Method Arr. R. Dany

Ø...... From [m] To [m] Method

mm mm

☐ Hand-drilled

Mud rotary

The Republic of Sudan Government of Southern Sudan

Ministry of Water Resources & Irrigation

Directorate of Rural Water Supply and Sanitation



	BOREHOLE COMPL			
PROJEC	Toroling of One Hand pump T ACTOR GTCAT Alile Astalling Cartofunding source	SHH Comp.	lete with In	Hallation.
CONTR	ACTOR GTCAT Alile Astalling Conterunding source	E PMU (And	112 EMENTED By	ACROSS (35D). ORG
le ID	Location State ANTERN KOUATORIBBORE N° 03 County KAPDETA EAST Payam NANYANGA CHOR Long. E 3U° 58' 57 Boma NABELENYUKUPELat. N° 05° 35'42 Village NABELENYUKUPELevation 1093 m° Site NABELENYUKUPE	·// ″ -3'4 "	Sketch map PN PN PN PN PN PN PN PN PN PN	A TO NAPIRIA
b Borehole ID	Use Community water supply Health facility Domestic water supply Education facility Community center Test well Private compound Property or handed over to ACR SS SS ST Sitting Geophysics Confical Stechical Sound Other :	2G · Ing	SITE 3 ' SITE 3 ' 10 Km from PEKIM and 19 Km from 2" site,	From
		Drilling consum	Approximate scale :	PEKIM
3	Drilling data Start date 31 2020 End date 01 09 2020 Total depth 104.5 [m] SWL 70 [m] Main water strike 88 [m] Yield 28 [m]	Diesel Engine Oil Hydraulic Oil	- [Lt] [Lt]	
	Dynamic water level SH.[m]	Hammer Oil		

Foam/polymer......[Lt]

	5 5 5	
tion .	Casing type ✓ uPVC ✓ Threaded	Filter pack (gravel pack) Composition
nstruc	Bottom plug Height above/below ground levelO[m] Plain casing & Screen installation inch	Grouting
ĉ Borehole construction	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	yes no <u>Cement</u> <u>M</u> ikolit Type From
bevelopment & pump testing	Duration. 1:5. [hr] Water: [Limpid] Turbi Comment fle Borehale your S Unfill allenr yield wers	atisfactorly developed
Development	Water level * H.a.g.l. = height above grou Measurement from H.a.g.l* = 0.55. [m. Test pumping Air-lift cap. Evaluation Step Drawdown Test Con. Duration [hr] Discharge 2.8 [m. 1]	stant RateTest-CRT Short CRT
o Pump & platform	Pump IM2 Afridev Submersible IM2 Marke Mono Duba Mono Mono Duba Mono Mono Comment Merch Image: Accep Well head and platform completion Melded on casing Fitt Apron Image: Concrete slab Image: Concrete slab	ed around casing
30		e borchote was entrefactorith red Construction ratio of 1:2:4
	Physical quality	Bacteriological quality
in .	Color Taste Turbidity [MTU] T° [°C] TDS [mg/lt] CE [µS/cm] Sample taken M Yes No Date Date	Faecal coliformcfu per 100 ml E. coli totalcfu per 100 ml Lab
Water quality	Comment Disinfection	
	Chemical used Nearest sources of possible contamination Type Remarks A.C.O. Sources of Courta	Distance

ちたいのうないのであったい

PUMP TES	T REPORT					
- Agenery (Contractory	000110000	- 11-1 001	Porchola no :	03.	
Location	Contractor: A	CROSS/GREA	DAILE DICON	Borehole no.: Submersible pump:	Falcon	
Site:		DELENYUKUP		Pump depth [m]:	95 M.	
Operator		Hen Turur	<u> </u>	Static water level [m]:	70.0	M
Date:	03/09/28	20		Starting test time:	8:30 am;	
Time [hh:mm]	Water Lever[m]	Drawdown [m]	Yield [l/min]	Remarks		Recovery [m]
00:00	70.00	0.00				84.00
00:01	70.48	Dille				83.32
00:02	70.96	0.96				82.64
00:03	71.44	1.44				81.96
00:04	71,92	1+92				81.28
00:05	72.40	2.40	2.8m74	Clear descharge		80.60
00:06	72.88	2.88		J		79.92
00:07	73.36	3.36				79.24
00:08	73.84	3.84				28.56
00:09	74.32	4+32				77.88
00:10	74.80	4.80				77.20
00:15	75-28	5-28				76.52
° 00:20	75-76	5.76				75.84
00:25	76.24	6.24				75.16
00:30	76.92	6.72	2.8mills	Clear discharge		74.48
00:35	77.20	7.20		J		7-3.80
00:40	77.68	7.68				73.12
00:45	78.16	8-16				72.44
00:50	78.64	8.64				71176
00:55	79.12	9:12		. ,		71.08
01:00	79.60	9.60	2-8m3/14	Clear discharge		71.04
01:10	80.08	10.08				
01:20	80.56	10-56				Jage R= 92.8
01:30	81.04	11.04				100
01;40	81.52	11-5-2				ufter 1Hr.
01:50	82.00	12.00				J
02:00	82.48	12.48	2.8milltr	Clew discharge		
02:15	82.96	12.96		J		
02:30	83.44	13-44			Pum	p test executed by:
02:45	83.92	13192				EAT NILE BRILLING
03:00	84.00	14.00	2.8m 1Hr	Clear discharge .	C	0.473.
03:15				0		C
03:30						
03:45						
04:00						

響 (L). 2

01 09/2020 **Borehole** completion date avith LCA dulle 1 Bor Comments 'n h for his 12 8m3PH C en is Iken.t pemp and -2 opr Cres ron D D due to deep sur recommen Intion em Catra vers mm

		Borehole Log and Construction Details	Constructions	Scale 10 cm : 10		
From	То	Lithology	Thik Ness	0M	7-0	BIH Car. 1. 5m Casing a.
) D	4-0	Reddish laterites with	_	10-		Gh
, t-0	120	Seme fers weathered granite voeks. Granisch fine gramed		80- 40-	د بر بر بر بر بر بر بر بر بر بر بر بر بر بر بر	- Gravel y
1-0	24-0	graditie gneise with Some few pebbles of Course grains Black/ gray Course grained	<u>-</u>	10250 67-	بر بر بر بر بر بر بر بر بر بر بر بر بر بر	
		ennphy bollifes. Grayish fine granned greeje	4,	70- 80-		-4"PVc pla Casings
	92-0	Allutish gray course ground quarte- drontes with first Had strike at 88 m :	-	90- 180		- 44" pve sen Cassings
12-0	1944	gramite vocks with some clark Coarse grains of	-	110-		chilled dept
		anne hur so Mitea from) 96 - 1940,				
			-			



BOREHOLE COMPLETION CERTIFICATE BE SIGNED BY: